

INTERACTIVE GLASS CHARGED SILICON FOR PERSON-ORIENTED  
DEVICE WITH IMPROVED TISSUE INTERACTION

By

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This dissertation is dedicated to  
my family without whose love and support I  
could not have done this task.

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# KEY TO SYMBOLS

## ABBREVI

Reactivity Index	I <sub>r</sub>
Calcium Phosphate Layer	CLP
Continued	on
Circular Hole Samples	C15
Cubic Centimeter (cc)	cc
Degree Centigrade	°C
Fourier Transform Infrared Spectroscopy	FTIR
Gase	g
Gel Permeation Chromatograph	GPC
Hydroxyapatite, Ca (OH) <sub>2</sub>	HAP
Hydroxycarbonate Apatite	HCA
Hydroxide ion	OH <sup>-</sup>
Inductively Coupled Plasma Spectroscopy	ICP
Liter	L
Micrometer (10 <sup>-6</sup> meter)	µm
Milliliter (10 <sup>-3</sup> liter)	mL
Millimeter (10 <sup>-3</sup> meter)	mm
Permeated Samples	PO
Polystyrene Sulfonate	PST
Polystyrene Sulfone	PSF
Polysulfonate Polyethylene	PST
Pretest (1 Torr = 1 mm mercury)	PreT
Radicalized Hole samples	RCH
Radicalized Body Fluid	RBF
1 : 1 Glass Radicalized Body Fluid	1:1RBF
Scanning Electron Microscopy	SEM
Surface Area to Volume Ratio	SA/V
Tetracycline	TTC
Thousand Electron Volts	keV
Tributylmethylammonium	TBAH
Weight to Volume Ratio	W/V
X-ray Photoelectron Spectroscopy	XPS

Abstract of Dissertation Presented to the Graduate School  
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**BIODIFFUSIVE GLASS COATED SILICONE FOR PROSTHETIC  
DEVICES WITH IMPROVED TISSUE INTERACTION**

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The discovery of bioactive glasses, in the early 1970s, has produced a material that develops a strong adherent bond with soft tissue. Many medical applications currently use silicone as an implant material, but are hindered by the formation of fibrous scar tissue surrounding the device. This fibrous scar tissue can lead to pain, infection, and/or extrusion of these devices. Bioactive ceramic materials are inherently brittle and can not be used in applications where a flexible material is needed. Therefore, the coating of existing flexible silicone medical devices, like catheters, with a bioactive glass material would give the advantages of both.

The research presented here is of methods used to coat silicon with a bioactive glass powder (Biosglass®) and the in vitro testing of these coatings. The bioactivity of these coatings was assessed using scanning electron microscopy, inductively coupled plasma spectroscopy, and Fourier transform infrared spectroscopy. It was observed that hydroxyapatite, a bone-like apatite, was formed in vitro on both the bioactive glass particles and the silicon surface between these particles. From these results a new theory was developed that related the distance between particles on a surface with the formation of an apatite layer. A critical distance between particles for the formation of an apatite layer on the substrate exists. This critical distance is a function of both the particle size and composition. In addition, a method to coat silicon catheters with bioactive glass powder is also discussed.

This coated catheter could ultimately be used for improved percutaneous access in peritoneal dialysis. The one barrier to peritoneal peritoneal dialysis was and the reason many patients switch from peritoneal to hemodialysis is recurrent exit-site infections and subsequent peritonitis. These infections are caused by the lack of a tight seal and overgrowth of microbial tissue around the catheter at the catheter-skin interface.

## CHAPTER 1 INTRODUCTION

The design of a percutaneous, through the skin, access device is one of the most challenging problems that faces the medical community today. The epidermis by its very nature is an effective barrier to access and will try to extrude or wall-off any foreign objects that penetrate it. Current medical devices that provide long-term percutaneous access for peritoneal dialysis, consist of catheters with fabric cuffs that are placed subcutaneous to anchor the device with scar tissue. The subcutaneous scar tissue formation is the healing process and provides an anchor for the device at the exit-site. During a longer term, the epidermal tissue healsin down around the catheter until it reaches the cuff size. This downgrowth provides access to bacteria and other pathogens that cause infection.

Despite the use of cuffs to limit the skin tract length, no catheter in use today can provide "significant prevention of exit-site/cannula infections" (Lewin, p.103) in peritoneal dialysis. The reduction of exit-site infections is considered an integral part of peritoneal dialysis.



adhesions (Yoshi, Feist, Sakai and Siffert). The healing pattern that forms around these devices, epithelial downgrowth, lacks soft tissue adhesion and the epithelium is observed to stop when it reaches the healing collagenous tissue at the device wall (Yoshi and Siffert).

Bioactive glasses have shown excellent soft tissue healing and adhesion (Moore and Gordon). This adhesion is attributed to the direct bonding of collagen fibers to the glass surface during hydroxyapatite formation (Ritter, Stoff, and Gordon). This apatite layer formed on the bioactive glass surface is the same phase as biological or bone-like apatite found in tissues (Ritter). While this study has mainly used Eucelux powders, the applications are general and should work for most any bioactive glass or glass-ceramic powder.

**HYPOXENIC** Coating silicone devices with a bioactive glass will allow for improved soft tissue adhesion without formation of an intervening fibrous capsule, stop or reduce the epithelial downgrowth, and create a better seal that prevents bacterial escape and infection.

## CHAPTER 1 BACKGROUND AND REVIEW OF LITERATURE

### 1.1 Percutaneous Devices

One of the most common percutaneous devices used today is the peritoneal dialysis (PD) catheter. This long-term indwelling catheter provides access to the peritoneal cavity for the exchange of dialysis fluids that clear the cavity of waste products (see Figure 1-1). The basic design and complications that exist with this device are shared with most other percutaneous-access devices and therefore this background will center on the design and complications associated with these types of catheters.

#### 1.1.1 Basic Design

A peritoneal dialysis catheter consists of a tube, usually made of silicone, that provides access through the skin to the peritoneal cavity. The intraperitoneal end of the catheter has multiple perforations and can be either straight, curled as disk shaped. The introduced portion of the catheter can also be either straight or curled (Mawardi).

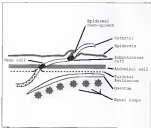


Figure 3-3: Cross section of a double cuff peritoneal dialysis catheter, showing preferred location of cuffs. (Adapted from Ashai)

The catheter may have either one or two lumens (registered trademark Supon, Wilmington, NH) fabric cuffs attached. The purpose of the cuffs is to stabilize the catheter by diffuse tissue ingrowth(5a)(6). The passageway formed by the catheter through the abdominal wall is defined as the tunnel. The number and position of the cuffs used determines what type of tunnel is formed (see Figure 3-2).

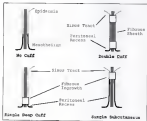


Figure 3-2. Stented structures form as a result of cuff positions. (Adapted from Tamm)

A single deep cuff would produce a long sinus tract of fibrin and be prone to exit-site infections. A single substantial cuff would produce a long Peritonial Abscess and be prone to pseudobulbaria. The use of a catheter with two cuffs (links) both of these and forms a tunnel with a short sinus tract, short peritoneal abscess, and a sheath of fibrous and fibrin covering the catheter segment between the two cuffs (Yardi). Authors have suggested that this double-cuff design is better at preventing infection, but thus far there have been no clinical studies that have resolved this issue (Hagfii). Other authors have concluded that the fibrous ingrowth of the catheter's cuff is the reason for their failure of the device (Yardi and Hagfii). Despite these ambiguities the majority of catheters used today consist of a double cuff design;

#### 2.1.2. Wound-Healing Around Peritoneal Catheters

During healing of a properly placed catheter, a blood clot first forms and fills the catheter cuff. This clot is slowly replaced by macrophages, fibroblasts and new capillaries. Macrophages surround the individual cuff fibers and collapse them around them. After 6 weeks healing, a strong fibrous tissue is formed throughout the cuff (Owen). Healing of the sinus tract begins with spiderweb cells spreading beneath the exit skin. These

cells continue to spread until they encounter epithelial cells from the opposite side or dense healthy collagen fibers (Mitsis, Kallits, and Kallits). This epithelial outgrowth is believed to be stopped by the dense fibrous tissue present in the Sarcosyl cuff (Mitsis and Kallits). The theory that dense collagen fibers inhibit epithelial outgrowth was first described by Hunter (Mitsis), and has led to development of percutaneous devices that encouraged large amounts of fibrous ingrowth (Kallits, Mitsis, and Hunter). Other researchers have made devices of silicone that are coated with a dense fibrous collagen (Chaffin and Chaffin), implanted percutaneously in rabbits where collagen immobilized implants show reduced bacterial infection at the exit-site (Chaffin).

### 2.2.3. Dressings

Many PD infections occurring early in the history of their usage, were caused either by poor catheter placement or lack of aseptic technique by patients during fluid changes. By positioning the catheter's tunnel in a downward direction at the exit point, sweat, dirt and pus can drain down, get rid away from the exit-site. Teaching the patient in proper aseptic technique and the use of improved "wedge-connector" ports has reduced the number of patient-related infections. These improvements have been associated with a

infection is the infection rate from 1 per patient month to 0.1 per patient year (Klein and Gagliardi, 1984), but, despite these improvements exit-site and tunnel infections are still a serious complication and are the major cause of catheter removal and mortality (Klein, 1984 and Gagliardi, 1984). The number of patients switching from PD to hemodialysis parallels the catheter-related rate (Klein, 1984). Studies indicate that 40% of children on PD switch to hemodialysis because of excessive and recurrent catheter-related infections (Gagliardi, 1984).

#### Catheter removal and tunneling

Exit-site/tunnel infections are a serious complication to peritoneal dialysis and most authors conclude that they infrequently initiate without catheter removal (Gagliardi and Kaji, 1981). Several studies have suggested that only the subcutaneous cuff need be removed (Chen and Kahn, 1981). In the latest study, the authors concluded that removal of the catheter's cuff in patients with persistent exit-site/tunnel infections can significantly reduce the rate of catheter loss associated with these infections (Kahn, 1981). These results suggested that the cuff, once infected, may become a depot for recurrent infections. Despite these complications, the benefits of cost, greater freedom and quality of life have resulted in a continued increase in the use of PD, at twice the rate of hemodialysis (Klein, 1984).

### 3.1.4 Growth of peritoneal dialysis

The growth of peritoneal dialysis has been dramatic over the 27 years of its existence. The increase has been from less than 5,000 patients worldwide in 1970 to more than 85,000 in 1996 (Blum and Nolph). The reasons for this rapid growth are the decrease in complication rates, the improved quality of life and increased freedom that PD offers a patient. The usage of PD varies widely for different countries and may be a factor of the reduced cost associated with PD. Third world countries have a very high percentage of their dialysis patients on PD, some have higher than 90% on PD (Gutierrez). One study concluded that home-based PD had a much lower cost associated with it compared to hospital-based hemodialysis (Dryden). The study found that hemodialysis had much higher physicians' fees, hospital cost and overhead costs than PD. The total annual costs, in Canadian dollars, of a typical PD treatment was 147,165 compared to a typical hemodialysis treatment cost of 476,023 (Dryden and Kishner).

#### Current research

It has been concluded that the problem of infection remains the major barrier to greater PD usage (Blum, Nolph, Ashby and Smith). This need for improved percutaneous access has encouraged research efforts into both coatings



and design changes. Percutaneous implants have been tested that are anchored to either the osseous or bony of animals (Janko and Janko). The authors concluded that stabilization of a percutaneous implant was a requirement for a successful percutaneous passage. Realizing that there are many percutaneous access situations which can not be anchored to bone, this group tested an access device consisting of a 3 cm by 4 cm sintered titanium fiber mesh implanted subcutaneously and then attached to a Teflon percutaneous component (Janko and Janko). Fiberous tissue ingrowth of the titanium mesh was intended to stabilize the implant. Early results with this implant showed that failure by tearing of the fiber mesh occurred in 33% of the animals at 4 months (Janko). In addition, epidermal overgrowth occurred along the Teflon component. Reinforcement of the titanium mesh at the attachment site reduced mesh failure to 33%, but significant epidermal overgrowth with cyst formation still occurred (Janko).

The use of metal antileakage coatings, such as silver, has also been the subject of research efforts. Bard Access Systems (Bard Lake Corp. WI) currently manufactures an antileakage cuff (Pitaball®) that is made of silver impregnated collagen. The porous collagen absorbs white implanted allowing for tissue ingrowth. Silver ions

leaching from the cuff provide antimicrobial activity. Clinical study of the effectiveness of Silacuff® used with central venous catheters concluded that catheter-related sepsis did not differ in frequency between these catheters and the control catheters (Smith). The antimicrobial activity occurs during the first 4 to 6 weeks (Smith). The Heire Corporation (Bedford, MA) has recently patented ion-beam deposition of silver as an antimicrobial coating on catheter surfaces. This coating is limited to only a few microns of the outer catheter surface and is currently being studied *in vivo* and in preliminary clinical trials (Smith). The use of antibiotic coatings are a suggested supplement to patient aseptic cleaning of the catheter site during early healing (Smith and Smith). It is unclear how effective these antibiotic coated devices will be over the long-term.

One experimental device that has successfully reduced the amount of epidermal overgrowth in percutaneous implantation is made of sintered hydroxyapatite (HAP).  $\text{Ca}_5(\text{PO}_4)_3\text{OH}$ , a calcium phosphate mineral, is a major component of bone. This material has been used in medicine and dentistry for more than 20 years (Smith). A comparative study between percutaneous devices made of HAP and silicone showed that the silicone devices had epidermal overgrowth that reached the bottom of the implant and a high rate of

infection and extrusion of the implant after only 3 months. RRP devices revealed limited epidermal overgrowth ( $\leq 1$  mm) at 3 months and a mild infection at 17 months (Ribe87). In an additional animal PD study, dogs survived for 432 days on PD using an RRP percutaneous-access device/catheter without exit-site infection (Ribe90). The authors of this later study observed a "tight and sterile seal between the RRP device and skin tissue" (Ribe87, p. 297 and Ribe90, p. 218). The suggestion that bioactive ceramics, like RRP, could be used to provide improved PD access has been made in recent review articles (Ribe81 and Gohl90).

### 3.1 Bioactive Ceramics

Bioactive may be characterized in one of three groups: inert, surface-active, and resorbable (Ribe82). Inert bioactive undergo almost no chemical change during implantation. Tissue response to these materials, much like that observed to silicon, is the formation of a fibrous scar capsule around the implant. Examples of inert bioactive are alumina and carbon. Resorbable bioactive, like calcium silicate, degrade gradually while implanted in the body and are slowly replaced by the surrounding tissue. The formation of a bond

Extensive bond between the material surface and the material is one of the intended functions of a surface-active bioactive glass. This bond is the result of a specific biological response at the tissue-implant interface.

### 1.1.3. Bioactive Glasses

In 1969 it was discovered by Hench and colleagues that ions could bond to certain glass compositions (Henf1). That group of bioactive glasses, called Bioglass<sup>®</sup>, are composed of  $\text{SiO}_2$ ,  $\text{Na}_2\text{O}$ ,  $\text{CaO}$  and  $\text{P}_2\text{O}_5$ . Later work by Wilson and Hench indicated that the most reactive glass composition, 60 to 62 mol%  $\text{SiO}_2$ , could develop an adherent bond to soft tissue (Wil90). Bioglass<sup>®</sup> 45B is the most studied composition and contains 45%  $\text{SiO}_2$ , 24.5%  $\text{Na}_2\text{O}$ , 24-25  $\text{CaO}$  and 4%  $\text{P}_2\text{O}_5$ , all in weight% (Bioglass<sup>®</sup> is a registered trademark of the University of Florida).

The basis of the bonding of bioactive glasses to tissue is a chemical reaction at the glass surface that results in the formation of an hydroxycarbonate apatite (HCA) layer in body fluids. These reactions occur on the glass surface when exposed to an aqueous solution; leaching, dissolution, and precipitation. These reactions have been extensively studied by researchers and are summarized by 5 reactions stages shown in Table 1-1 (Henf1a). During the leaching reaction stage 1), an ion exchange with  $\text{H}^+$  or  $\text{H}_3\text{O}^+$ , is

reaction, covers the release of alkali or alkaline earth elements from the glass surface into the surrounding fluid.

Table 2-2. Reaction stages of bioactive glass [Henrici]-

Stage	
1	Rapid ion exchange of $\text{Na}^+$ , $\text{Ca}^{2+}$ , or $\text{Sr}^{2+}$ with $\text{H}^+$ as $\text{H}_2\text{O}$ $\text{Si-O-Na}^+ + \text{H}^+ \rightarrow \text{Si-OH} + \text{Na}^+$
2	Breaking of Si-O-Si bonds resulting in the loss of soluble silica in the form of $\text{Si}(\text{OH})_4$ and the formation of Si-OH on the glass surface $\text{Si-O-Si} + \text{H}_2\text{O} \rightarrow \text{Si-OH} + \text{Si-OH}$
3	Condensation and repolymerization of silica-rich layer on the surface $\text{O-Si-OH} + \text{HO-Si-O} \rightarrow \text{O-Si-O-Si-O} + \text{H}_2\text{O}$
4	Migration of $\text{Ca}^{2+}$ and $\text{PO}_4^{3-}$ groups through the silica-rich layer to the surface forming a $\text{CaO-P}_2\text{O}_5$ -rich film, followed by growth of the amorphous $\text{CaO-P}_2\text{O}_5$ -rich film by incorporation of soluble calcium and phosphate from solution.
5	Crystallization of the amorphous $\text{CaO-P}_2\text{O}_5$ film by liberation of $\text{OH}^-$ or $\text{H}_2\text{O}^+$ from solution to form hydroxyl or carbonate apatite layers.

These network-modifying ions are not part of the glass network and are rapidly released causing an increase in the interfacial pH. Stage 2, involves the breaking of the silica glass network bonds ( $\text{O-Si-O-Si-O-Si-O}$ ) causing the dissolution of silica into solution in the form of silicic acid [ $\text{Si}(\text{OH})_4$ ]. The rate of this dissolution is a function of

the number of bridging oxygen bonds in the glass network and is extremely slow for compositions of 44-51  $\text{SiO}_2$ . Stages 1 and 2 are reactions that occur simultaneously at the glass-water interface (Stahl). The resulting silanols on the surface of the glass react by polycondensation to form a silica-rich gel layer (Stage 3). In Stage 4, a precipitation reaction takes place, calcium and phosphate ions migrate to the surface of the glass and along with those in solution form an amorphous calcium-phosphate layer (CaP) on and within the silica-rich gel. This CaP layer crystallizes to hydroxyapatite apatite (HCA) by incorporating  $\text{OH}^-$  anions and water from solution.

The reactions that occur during these 4 stages can be monitored by using Fourier Transform infrared reflection (FTIR) spectroscopy. FTIR analysis reveals the types and amount of molecular bonds that are present at the glass surface. Several review papers have summarized the use of FTIR analysis to monitor these changes on bioactive glass surfaces (Stahl, Clark, Kokubo and Hench). Due to the scattering induced by the uneven texture of the HCA surface layer formed, diffuse infrared reflectance, rather than specular reflectance, is used to analyze these glasses (Stahl). An example of FTIR analysis of bioactive glasses soaked in Tris buffer for 0, 1, and 2 hours at 37°C are

shown in Figure 3-1. The amorphous CaP and silicocal layer are seen at 1 hour. Crystalline HCA is seen at 2 hours.

The molecular bond vibrations that are of interest in the analysis of bioactive glasses are Si-O-Si stretching and bending vibrations, indicative of a silicocal layer; and P-O stretching and bending vibrations, indicative of a calcium phosphate layer. Indicative of the transformation of HSR to an HCA layer on the surface, these P-O bending vibrations split from 1 amorphous band near  $560\text{ cm}^{-1}$  to 3 crystalline bands at  $450$ ,  $574$  and  $598\text{ cm}^{-1}$ . The infrared frequencies and band assignments of these molecular bonds have been established for bioactive glass reactions and are shown in Table 3-2 (Hendler). This table depicts the surface changes on 45S5 Bioglass® with reaction time in Tris buffer.

This HCA layer formed on bioactive glasses is the same phase as biological apatite formed in tissue and is necessary for the formation of a bond with tissue to occur (Hendler). The rate of its formation has been used to evaluate the bioactivity index ( $I_b$ ) of various glasses (Hendler). During the precipitation reaction collagen fibrils, present near the glass surface, are incorporated within the HCA layer and result in a bonding of tissue to the glass surface (Hendler).

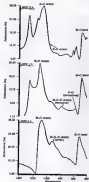


Figure 2-3 IR spectra of a film of hexamethyldisilazane after 0, 1 and 3 hours in TMS vapor at 37°C (Reed 11).





### 3.1.3. Soft Tissue Interactions

Some of the evidence of soft tissue bonding to Bioglass® came from a comparative study of materials used in facial augmentation (Willett). In this study of adult dogs, Bioglass® was shown to bond macroscopically to soft tissue (overlying nasal, maxilla and chin facial bones). It was so firmly bonded that the tissue had to "be forcibly stripped" (Willett, p. 144) from the samples to remove it. Willett samples at these same sites eroded the underlying bone and developed a thin, non-adherent fibrous capsule. Other studies have confirmed this direct soft tissue adhesion to Bioglass® and not normal substances, not intramuscular and even to surgical to Bioglass®, without the formation of a fibrous capsule (Willett, Hoff, and Neenan). In all of these studies, evidence of direct attachment of collagen fibrils to the glass surface was noted.

Bioglass® has been used to manufacture commercially available middle ear prosthetic devices for the treatment of hearing loss. These devices provide a connection between the soft connective tissues of the tympanic membrane and the oval window, replacing the ossicles. A major mode of failure of implants made of other materials is extrusion through the tympanic membrane (Willett). Devices made of Bioglass® bond to the soft tissue of the tympanic membrane,

simulating that mode of failure, and have been in use clinically for 15 years (Wille). Another clinical success of bioinert bonding is soft tissue as with endosseous ridge maintenance implants. These osseous devices are placed in the alveolar ridge after tooth extraction to maintain ridge morphology (Wille). These implants have also been clinically used for several years and have been shown to bond to the soft connective tissue of gingiva by collagen fibers bonding within the silica-gel/BSA layer on the surface of the implant (Wille and Wille).

#### 2.2.2. Bioactive Ceramic Coatings

Some of the earliest coating applications of bioinert were on metal femoral implants. These coatings were either dip coated from sol-gel glass, flame-spray coated or fired onto the metal with an enamel frit/BSA and Baritic. These techniques use very high temperatures to melt the glass onto the substrate, produce brittle coatings and are not suitable to coat polymer substrates.

The precipitation of a bone-like apatite layer on a polymer surface is not a trivial mission. Polymers can have highly hydrophobic surfaces that inherently repel the hydrophilic, concentrated calcium phosphate solutions that are used in the precipitation of HA on a surface. Experiments in our lab have shown that these solutions will not spread

usually 2-40 nm, silicon surface, and when dried onto a silicon substrate, they are inherently brittle and will flake off after repeated bending of the substrate.

One research group has tried modifying the surfaces of polymer substrates by adding sulfonated or phosphoryl-*o*-grouped polymers and then immersing them in calcium phosphate aqueous solutions (CaHPO<sub>4</sub>, CaHPO<sub>3</sub>, and CaH<sub>2</sub>P<sub>2</sub>O<sub>7</sub>). The presence of phosphate groups on the surface of the substrate has induced the precipitation of hydroxyapatite (HAP) and the sulfonated surfaces were strong adsorbents of calcium ions (Hosaka). Polymers were saturated with calcium prior to immersion and would induce the formation of crystals of calcium carbonate monohydrate, but not hydroxyapatite or tricalcium phosphate (CaHPO<sub>4</sub>).

A method detailing the precipitation of nonionic calcium phosphate and hydroxyapatite films on a variety of substrates has been introduced (Muller). This method involved the placement of a substrate in a face-to-face orientation in a birefringent glass plate. Fluorescophore maintained a constant distance of 0.5 nm between the substrate and glass plate. This combination was immersed in a simulated body fluid (SBF) for 7 days, separated, gently washed with ion-exchange and distilled water, and dried. Re-immersion of the substrate in a solution containing 1.5

than the ion concentrations in HEP (3-5M $\Omega$ ) for an additional 7 days, caused the formation of a continuous apatite layer (1  $\mu$ m thick) on the surface that had been facing the bioactive glass. Increasing the distance between the substrate and glass during the first immersion reduced the amount of apatite formed and no apatite was formed at a distance greater than 1 cm. The authors concluded that the mechanism of apatite coating was 1) dissolution from dissolving from the glass and adsorbing on the substrate, 2) apatite nucleation on the adsorbed silicate ions, and 3) apatite crystal growth on the substrate by using ions from the HEP (3-5M $\Omega$ ). Distinct uncoated areas were present in the location of where the alumina spacers had been during the first treatment.

A refinement of the technique by the same group included placing the substrate on a bed of bioactive glass particles during the first immersion in HEP. This process was described as a "Wickonite Method" (Tachii, p. 2803) for forming a bone-like apatite layer. The authors tested the adhesive strength of a bone-like apatite layer grown on 30 different types of polymer substrates. The first immersion, face down on top of glass particles, was in HEP for 4 days and was followed by a second immersion, without glass particles, in the 1.5M $\Omega$  solution for an additional 4 days.

if the first step was omitted, the apatite did not form during the second treatment (Tami). Although silicone was included as one of the polymers to be tested, data on the adhesive strength or the coating process was omitted from the discussion (all other polymers were excluded) (Tami). No reason for this omission was given by the authors. The polymers which showed the greatest adhesive strengths were polyethylene terephthalate (PET) and polydimethylsiloxane (PDMS); the authors attributed this strength to chemical bonding between the apatite layer and the polymer's ester and silyl groups, respectively (Tami). The proposed mechanism of apatite coating on the substrate was the same as discussed in the previous publication (Mami). Small increases in the adhesive strength could be made for polymers such as PET and polymethyl methacrylate if the substrate were pretreated in 1 N HCl prior to the first step (Tami). This pre-treatment increased the number of polar groups on the surface of the substrate as measured by X-ray photoelectron spectroscopy (XPS) (Tami). These polar groups were intended to improve the bonding of apatite to the surface. Although the use of bioactive glass powder silicified the untreated areas where alumina spacers had been in the previous study (Mami), only 1 side of the substrate was coated with the thin (0.3  $\mu$ m) apatite layer (Tami).

One technique to coat the ureter implant is a paired layer deposition discussed in a recent study (Hartig). A thin amorphous film of MBP was applied to the surface of a silicone tubing. The film was measured between 0.5 to 1  $\mu$  in thickness and could be applied in a selected area (Table and text). The coating was continuous, except for cracks that formed when the tubing was bent. It is unclear how this cracked, amorphous and extremely thin coating will react as a permanent application.

#### 3.1.1 Attempts at Sol-gel Coating

Several unsuccessful attempts were made in our lab to coat silicone with a layer of sol-gel derived bioactive glass. A bioactive glass sol was made by mixing Tetraethoxysilane (TEOS), Triethyl phosphate, Calcium nitrate pentahydrate, Nitric acid, distilled water and ethanol using a formula published by us (Table). The coating of silicone with sol-gel derived bioactive glasses suffered from two major difficulties. 1) the spread on hydrophilic sol had very tiny islands of glass on the surface of a cured silicone sheet rather than an even coating. Further, these islands inherently had a large surface area and surface area, complete dissolution of the islands was observed in as short a time as 12 hours in water at 37°C. 2) the high acid content of the sol interfered with

The functionalizing of the siloxane when mixed with two-part epoxies,<sup>1</sup> thus resulted in bubbles and voids in the sheeting. In an act of desperation, melt-derived borosilicate glass (Diboglass) (3M, 720-10 µm granules, 3-5- Biomaterials, Alachua, FL) powder was pressed onto the surface of a siloxane sheet 3 hours into the curing reaction. The results of an x-ray tracing of these samples, called "x-ray-prime", showed the formation of MMA both on the glass particles and between the particles on the siloxane surface. These results concurred with those of other researchers at about the same time. Investigators found that PMEP/borosilicate glass composite surfaces could precipitate MMA both on the glass reinforcing phase and the polymer between the glass phase (Barts and Barts).



## CHAPTER 2 MATERIALS AND METHODS

### 2.1 Preparation of Silicone Sheets

Silicone sheets were made by casting a solution of 100-part silicone (Dow-Silux SX-1400, Lot 427144, Dowcor Silicone Inc., Akron, Ohio) benzene onto a glass plate and then curing the silicone in a vacuum oven. A 1:1 ratio silicone/benzene solution is made by weighing 10.0 g of each silicone part into a 50 cc disposable centrifuge tube (Fisherbrand®; Fisher Scientific, Pittsburgh, PA) and then mixing this with 10 ml of benzene (Optima grade, Fisher Scientific, Fair Lawn, NJ) on a rotary mixer for 1 hour. This silicone/benzene solution was poured onto a glass plate (12 in x 6 in) that had a border made of disposable glass tape glued to the plate with commercial silicone caulk. The benzene was allowed to evaporate in a hood at room temperature and then the plate was placed in a vacuum oven (National Appliance Co., Portland, OR) pumped down to 10 Torr for 1 hour and then held at 10 Torr over-night at 70°C. The first hour of pumping insured that all entrapped air was

removed from the silicon. The remaining sheet of silicon was removed from the glass plate and cut into smaller squares (5 cm x 5 cm) for coating with bioactive powder.

### 3.1. Preparation of Buffers

Two types of buffers were made and used during the *in vitro* testing of these samples: 1) a simulated body fluid (SBF) buffer and 2) a Tris buffered solution. The SBF was described by Kokubo for the *in vitro* testing of bioactive glasses (Kokubo) as having similar ion concentrations and pH as human blood plasma. The SBF was buffered to pH 7.35 with tri(hydroxymethyl) aminomethane (THAM) and hydrochloric acid (HCl) at 37°C. The SBF was made by adding the reagents, shown below in Table 3-1, to 4 L of distilled water.

Table 3-1: Reagents used for preparing 4 L of SBF.

Reagent	Amount
NaCl	85.084 g
NaHCO <sub>3</sub>	1.096 g
KCl	8.894 g
CaCl <sub>2</sub>	2.489 g
NaCl 45x3	0.833 g
1M - HCl	100 mL
THAM	1.103 g
Na <sub>2</sub> SO <sub>4</sub>	2.354 g
1M (Na <sub>2</sub> SO <sub>4</sub> ) (THAM)	10.029 g

Once the samples are obtained and the solution is brought to TPC, the pH is adjusted to 7.20 by adding very small amounts of either TBAH or 1 N HCl. This buffer solution was made by using only TBAH and HCl.

### 3.1. Coating Methods

#### 3.1.1. Basic coating of Silicon Wafer

Mixing of a sample of two-part silicone as described in section 3.1 was followed by placement in a vacuum oven with pumping down to 18 Torr at TPC for 1 hour to remove the entrapped air bubbles. Then 2 g of adhesive glass powder (Kilb Stogdiner, 700-40 40 diameter, lot# 7402, 2.5 Dimeterials Inc., Atlanta, FL) was spread with a glass microscope slide onto the silicone surface. The powder was pressed into the tacky, partially cured surface gently with the glass slide and the glass plate placed back into the vacuum oven under 18 Torr of vacuum at TPC for 24 hours. A rectangular piece of this sample (1 cm by 2 cm) was exposed to 30 mW of IRF at TPC for 18 days. After that period, the sample was removed, rinsed with acetone, and allowed to air dry at room temperature in a desiccator. The surface of the treated sample was analyzed using Fourier Transform Infrared (FTIR) spectroscopy using a diffuse reflection

steps. Each of the reacted samples was coated with gold/palladium and imaged using low voltage (2 kV) scanning electron microscopy (SEM).

#### Varied amounts of powder

Seven squares, 5 cm by 5 cm, were cut from a piece of silicone sheeting prepared using the technique described section 3.1. These squares were soaked in hexane for 2 hours to remove most of the oils in the sheeting. Once dry, the squares were placed flat on a clean glass plate. A solution of two-part silicone/hexane was made by weighing out equal amounts of each part of silicone into a centrifuge tube and then adding enough hexane to make a 10% (silicone weight/ hexane volume) solution. This 10% silicone/hexane solution was allowed to mix in a tube vortexer for 1 hour. Using a 1 mL quartz pipet, 1 mL of this solution was applied evenly to the surface of each silicone square and the hexane allowed to evaporate. This produced a thin layer of uncured silicone on the surface of each square. A weighed amount (0.1, 0.2, 0.3, 0.4 and 0.5 g) of bioactive glass (40B Bioglass, 120-125  $\mu$ m diameter, Lot# V001) powder was evenly applied to each square using a "ball shaker"-like device made out of a 600 mL Oscatori Acoustar Co., Lafayetteville, GA) with several balls (3 mm each) punched into the Teflon septa. Each square was then placed between two Teflon

smoothly and pressed in a heated carbon press at 100°C to 1000 psi for 1 hour. The smooth sample, labeled B1, was coated with the thin layer of uncured silicone and 4.5 g of glass powder using the above technique but, was heated in a vacuum oven at 10 Torr and 70°C for 24 hours and not pressed. Cross-sectional micrographs were taken of samples from each square using SEM. Cross-sectional samples from each square were broken after freezing in liquid nitrogen for 2 minutes. Sixteen disks, 1 cm diameter, were cut from each square using a standard rock-chisel. These disks were then placed in 15 ml centrifuge tubes (Fisherbrand®). At the appropriate time, 8 ml of HEP was added to each tube, the tube sealed and placed in a constant temperature shaker bath (American Optical, Model 80013, Buffalo, NY) at 37°C. One tube was removed at 10 minutes and 1, 2, 4, and 12 hours. This provided a coated surface area to solution volume (CM<sup>2</sup>/V) ratio of 8 l cm<sup>3</sup>. After samples were retrieved, they were removed from the HEP with tweezers, submerged in Arcton (Optima grade, Fisher Scientific, Fair Lawn, NJ) for 1 minute, gently removed, allowed to air dry at room temperature on a lint-free tissue (Kimwipe EX-4, Kimberly-Clark Corp., Lowell, MA) and placed in labeled polyethylene dishes. The solution was replaced in the temperature bath for 1 hour to return to 37°C and the pH of the solution

measured with a probe that had been calibrated using pH standards that were also at 37°C. Measurement was carried out while still in the constant temperature bath, then the solution was sealed and stored for inductively coupled plasma (ICP) spectroscopy analysis for the elemental concentration of phosphorus (P), silicon (Si), and calcium (Ca) in solution. The measured surface of each disk was analyzed using FTIR.

#### Test of "leaky" effect

Three squares, 5 cm by 5 cm, were cut from a silicone sheet, soaked in heptane, dried, and placed on a glass glass plate as described above. A 50% (w/v) silicone/heptane solution was made and allowed to mix on a table vibrator for 1 hour. Using a 1 mL glass pipet, 0.5 mL of this solution was applied evenly to the surface of one silicone square and the heptane was allowed to evaporate. This produced a thin layer of unreacted silicone on the surface of each square. Sixteen disks, 1 cm diameter, were cut from this coated sheet. A short piece of glass tubing, 0.5 cm internal diameter, was gently placed in the center of a coated disk. Fluorescing glass (Fisher Hinglamb, 1/8-3/8 cm diameter, Lot# V100) powder was placed down the short glass tube. A vacuum was applied to the glass tube, using a vacuum pump and a rubber hose, to remove any unattached fluorescent glass particles. The glass

was partially covered, leaving a 0.5 cm diameter section of bioactive glass coated silicone in the dish's center. This procedure was repeated for each dish using a new glass tube each time. The dishes were placed on a glass plate and cured in a vacuum oven at 10 Torr and 70°C for 24 hours. These samples were labeled "C1P". To the other two squares, 0-1 ml of the 10% silicone/hexanes solution was applied to a 0.5 cm wide section of two sides of each square. The remainder of the square was sealed from coating by placing a glass microscope slide on the surfaces of the square. The hexanes were allowed to evaporate and bioactive glass powder, as in C1P, was dropped onto the exposed silicone area. The squares were then placed in a vacuum oven at 10 Torr and 70°C for 24 hours. After the silicone cured, the glass microscope slides were removed from the squares and excess bioactive glass powder was raised from the squares with acetone. From each of these two squares, 8 samples were cut in the shape of rectangles 1 cm by 2 cm with a bioactive glass coated end that measured 1 cm by 0.5 cm. These rectangular samples were labeled "R1P". A diagram of each of these samples is shown in Figure 3-1. Each pair of samples were placed in 20 ml centrifuge tubes for bioactivity testing. At the appropriate time for samples at 0, 1, 3, 10, and 20 days, 0 ml of DMF was added to each tube



Figure 3-10 Diagram of C13 and R13 samples

containing a C13 sample and 15 mL of RNF was added to tubes containing a R13 sample. The tubes were sealed and placed in a constant temperature shaker bath at 37°C (3 samples at each time period). These separate RNF volumes maintained a coated surface area to solution volume (SA/V) ratio of 1:1.0.

After samples were reacted, they were removed from the RNF, submerged in acetone for 1 minute, removed and allowed to dry on a fume-free tissue. The solution was replaced in the temperature bath for pH measurement of the solution at 37°C. The solution was cooled and stored for HPLC analysis. The reacted surface of each sample was analyzed using FTIR spectroscopy and low voltage SEM.



### Fine bioactive glass powder

Six squares, 5 cm by 5 cm, were cut from a sheet of silicone, soaked in hexane, dried, and placed on a glass plate as described above. Using a micropipeter (Biorad Transfer, Oxford, Tex., St. Louis, MO) 2.15 ml of a 10% silicone/hexane solution was applied to one end of 3 squares and spread across each square using a glass microscope slide. Once the hexane evaporated, a very thin layer of etched silicone remained on each of the 3 squares. The following 3 sizes of fine bioactive glass powder (Biomaterials, Biotech, FL) were applied to each to both an uncoated square and a coated square: 1) 45 $\mu$  BioGlass, 45  $\mu$ m powder, Lot# 5100; 2) 45 $\mu$  BioGlass, 45  $\mu$ m powder, Lot# 5012; and 3) 45 $\mu$  BioGlass, 45  $\mu$ m powder, Lot# 5048. The glass powder was spread onto each square using a glass microscope slide. All 6 squares were then placed in a vacuum oven at 10 Torr and 70°C for 24 hours. Disks, 1 cm diameter, were cut from each of the squares and placed in labeled 15ml centrifuge tubes. At the appropriate time, 8 ml of DMF was added to each tube containing, the tube sealed and placed in a constant temperature shaker bath at 37°C for 0, 1, 3, 12, and 24 hours (3 samples at each time period). In addition, 3 disks of untreated silicone were treated to 8 ml of DMF at 37°C for 1 and 24 hours. After samples were

removed, they were removed from the BPF, submerged in acetone for 1 minute, removed and allowed to air dry at room temperature on a lint-free tissue. The solution was replaced in the temperature bath for pH measurement of the solution at 10°C. The solution was sealed and saved for IRF analysis. The coated surface of one sample from each type was analyzed using FTIR diffuse reflection spectroscopy.

#### 4.3.2 Mask Coating of Substrate

Spectra/Mask® woven nylon mask plates (Spectra Medical Industries, Inc., Boston, MA), commonly used for filtration, were used to mask the surface of silicone squares coated with uncoated silicone providing a pattern of powder on the surface of the silicone squares.

#### IL-6000

One square, 5 cm by 5 cm, was cut from a sheet of silicone, soaked in hexane, dried, and placed on a glass plate as previously described. Using a micropipetter 0.15  $\mu$ l of a 10% (w/v) silicone/hexane solution was applied to one end of the square and spread using a glass microscope slide once the hexane evaporated, a piece of 70  $\mu$ m Spectra/Mask® (DART 00000, 70  $\mu$ m square holes separated by 70  $\mu$ m wide threads of nylon), 5 cm by 5 cm, was gently applied on top of the uncoated silicone layer. Biorivine glass powder (Silica

Bioglass®; 125-83  $\mu\text{m}$  diameter, Lot# 8100) was spread onto this washed surface. Once the glass powder had filled all of the pores in the mesh, the excess glass was gently blown off using compressed dry air. The spin mesh was removed leaving a pattern of single glass particles evenly spaced. The square was placed in the vacuum oven at 10 Torr and 10°C for 24 hours. Disks of 1 cm diameter were cut from these squares and placed into 15 mL centrifuge tubes. Eight milliliters of DBF was added to each tube. The tube was sealed and placed in a constant temperature shaker bath at 37°C for 0, 1, 3, 7, 12 and 24 hours (2 samples at each time period). In addition, single disks were reacted in DBF for 1, 2, 5 and 10 days at 37°C. After samples were reacted, they were removed from the DBF, submerged in acetone for 1 minute, removed and allowed to dry on a lint-free towel. The pH of the solution was measured at 37°C, the solution saved for DBF analysis, and the reacted surfaces analyzed using FTIR spectroscopy and low voltage SEM.

#### 20/80, 75/25, 10/90, & 20/80 samples

Using the same technique described in 12.2.2.1 above, 2 square mesh were coated with a pattern of the following bioactive glass powders: 1) 45S Bioglass®, 125-83  $\mu\text{m}$  diameter, Lot# 8108, 2) 5S Bioglass®, 80-83  $\mu\text{m}$  diameter, Lot# 8100, 3) 5S Bioglass®, 80-83  $\mu\text{m}$  diameter, Lot# 8100,

is 99% fluorinated, 200  $\mu$ m diameter, Lark Glass. These glass products are of different composition and exhibit different reactions *in vivo*. The coated squares were placed in a vacuum oven at 18 torr and 70°C for 24 hours. Disks of 1 cm diameter were cut from these squares and placed into labeled 15 ml centrifuge tubes. Disks were reacted with 8 ml of Tris buffer and 8HF at 37°C for 1, 2, 3, 10 and 12 hours in a constant temperature shaking bath. In addition, 2 uncoated 1 cm disks were also reacted in 8HF at the same time periods. The reacted samples were removed from their solutions, submerged in acetone for 1 minute, removed and allowed to dry on a lint free tissue. The pH of the solution was measured at 37°C, the solution saved for HPLC analysis, and the reacted surfaces analyzed using FTIR spectroscopy and low voltage SEM.

### 3.1.3. Dip-Coating of Catheters

Samples, 5 cm long, of an all-silicone Foley catheter (18 French, Bard Access) were cut and then washed in hexane for 2 hours (including the balloon and distal snare). After the catheter pieces were allowed to dry, they were placed in a 50 ml centrifuge tube that contained 30 ml of a 25% silicon/toluene solution (1.3 g of two-part silicone and fill with toluene to 30 ml). Two catheter pieces were placed in this solution for 2 hours at room temperature. Then the

Collectors were removed and placed on heat paper strips to allow the excess dipping solution to drip off and the solvent to evaporate (see diagram of process in Figure 3-21). After 1 hour, the ends of the catheter pieces are masked-off by placing tape around each end and crimping the tape-ends. The masked catheter pieces are then placed in a 15 ml centrifuge tube that containing 10 g of fine-grained glass (45 $\mu$ m Sphéron 65, 125-150  $\mu$ m diameter, Lot# V1002) powder. By rotating the tube parallel to the floor, all sides of the catheter are coated with powder. Once coated with powder, the catheter pieces were removed from the centrifuge tube and the tape carefully removed. The powder was pressed into the surface of the catheter piece by rubbing it on a glass plate with a microscope slide. The catheter pieces were placed in EPC vials to hold them upright and heated in the vacuum oven at 10 Torr and 30°C for 24 hours. SEM images of catheter powder coated brushes with liquid nitrogen were taken to view the cross-section.

### 3.3 Surface Analysis

The treated surface of each sample was analyzed using Fourier transform infrared (FTIR) spectroscopy and low voltage (2 kV) scanning electron microscopy (SEM).

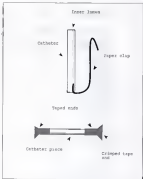


Figure 3-3) Diagram of methods used to tape and mask catheter places for dip coating with silicone.

### 1.1.1. FTIR

The surface of reacted samples was analyzed using Fourier transform infrared (FTIR) spectroscopy using a diffuse reflection stage (Model 2000, Nicolet Instruments Corp., Madison, WI). Diffuse infrared reflectance was chosen due to the large amount of scattering induced by the irregular glass powder coating the surface of these samples, the poor IR transmission qualities of silicon, and the fact that this technique has been used by many researchers to study the reaction surfaces of bioactive glasses (Chen, Kokubo, Henri, and Hiroki). Samples were placed on the diffuse stage and the IR beam focused for the best reflection intensity.

### 1.1.2. SEM

Half an quarter pieces of each reacted sample were cut with a scalpel blade and mounted on aluminum SEM stubs with cyanoacrylate glue (SuperGlue). Samples were grounded to the stubs by using carbon paint and the stub coated with a very thin layer of gold/palladium using a sputter coater (2 minutes coating time). Samples were analyzed by low voltage (2 kV) SEM (model JSM-6100, Bedford, MA) and representative photos of each surface were taken using Polaroid Type 66 485 Instant Sheet Film (Polaroid, Cambridge, MA).

## 3.5. Solution Analysis

### 3.5.1 solution pH

After removal of the reacted sample, the solution was replaced in the temperature bath for 1 hour to return to 37°C. The pH of the solution was measured (Corning pH Meter, Model 105, Corning, NY) with a probe (Corning Combination Electrode, Fisher Scientific, Atlanta, GA) that had been calibrated using pH standards (Fisher Scientific, Atlanta, GA) at 37°C.

### 3.5.2 elemental concentrations

The elemental concentrations of phosphorus (P), silicon (Si), and calcium (Ca) in solution were measured using inductively coupled plasma (ICP) atomic emission spectroscopy using a Plasma 80 (Perkin-Elmer, Norwalk, CT). ICP is an atomic emission technique that measures the concentration of elements in an aqueous solution by using a plasma torch to ignite a fine mist of solution. The solution sample was introduced into the instrument through a nebulizing tube by means of a peristaltic pump. A nebulizer converts the liquid to a fine aerosol which is sprayed into the plasma. The spectrum of light emitted from this aerosol is characteristic of the elements in solution.



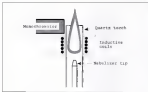


Figure 3-1 ICP torch configuration.

Each element emits a unique set of wavelengths of light and the concentration of that element is directly proportional to the intensity of those emitted wavelengths. By using standard concentration solutions and careful volumetric dilutions, a standard curve relating the intensity to the concentration can be plotted.

An ICP method was created to measure the concentrations of elemental P, Si and Ca in solutions reacted with coated silicon samples. The emission wavelengths of each element were chosen from established tables (MUSK, photomultiplier tube (PMT) voltage and element scan times that allowed accurate measurement. Parameters are shown in Table 3-2.

Table 3-7) ICP parameters used

Element	Wave length (nm)	Element time (seconds)	RF voltage (V)
Phosphorus	213.42	10.00	400
Silicon	235.14	8.00	400
Calcium	285.37	10.00	300

Two standard solutions were made using 1000 ppm Icp Plasma standards (Icpa Chemical, Metuchen, NJ) of phosphorus (lot no. 3-1100), silicon (lot no. 4-1000) and calcium (lot no. 4-2000). Standards were made using glass & volumetric flasks and pipes, diluted with ultra-pure water. Standards consisted of 100 and 50 ppm P; 100 and 10 ppm Si, and 100 and 100 ppm Ca. A blank solution of ultra-pure water was also used. Standards and the blank were run and the instrument calculated a linear standard curve (intensity vs. concentration). Correlation coefficients of these standard curves varied between 0.999 and 1.000. The concentrations of each element in solution was calculated using these standard curves and reported as ppm. Three measurements were taken of each solution and the mean and standard deviation calculated and reported by the instrument. When the blank was run as a sample the values obtained were 0.2 ppm P, 0 ppm Si, and 0 ppm Ca. Detection limits exist for these are 0.2 ppm P, 0.01 ppm Si, and 0.2 ppm Ca (HALL).

## CHAPTER 4 RESULTS AND DISCUSSION

### 4.1. Sol-Gel Process

After the number of failed attempts at coating silicones with sol-gel derived inorganic glass, it was a pleasant surprise to find that a coating made of sol-derived glass powder (named "5/5/Trace") was both stable in a simulated body fluid (SBF) buffer for 18 days and formed an apatite layer on the surface. Analysis of the reacted surface, by Fourier Transform Infrared (FTIR) spectroscopy, showed that a hydroxycarbonate apatite (HCA) layer had formed on the surface after 18 days reaction (see Figure 4-1). Figure 4-1 shows a comparison between FTIR spectra obtained from the KBr-diluted glass powder coated sample and an uncoated silicone disk reacted in SBF for 18 days at 37°C. The spectrum from the coated sample (top spectrum) show the characteristic peaks of a HCA layer on the reacted surface: 3 narrow peaks near 318, 314, and 346  $\text{cm}^{-1}$  and a broad peak at 1080  $\text{cm}^{-1}$ , representing the P-O asymmetric bending vibration and P-O stretching vibrations, respectively.

(Mar71). The uncoated sample (Mar70) shows a result for silicone: a narrow peak at  $1250\text{ cm}^{-1}$  representing Si-CH<sub>3</sub> bending, 2 peaks at  $1190$  and  $1090\text{ cm}^{-1}$  representing Si-O stretching, and a strong peak at  $980\text{ cm}^{-1}$  representing the Si-O-Si tetrahedral bending.

When the treated surface of the L/S/Freez sample was imaged using low voltage (2 kV) scanning electron microscopy (SEM) an interesting result was seen. Not only did the BSA layer precipitate on the bioactive glass particles, but it also formed on the silicone polymer surface between particles of bioactive glass (see Figure 2-2). This result corresponded to observations by other researchers testing composites made of bioactive glasses and engineering thermoplastic (i.e., polyethylene and PEEK) at the same time (Mar71, Mar72 and Mar74). The success of this sample coating technique, implied a great change from sol-gel derived coating to sol-derived powder coating of silicone surfaces. Glass powder used to coat the L/S/Freez sample was of a very coarse size ( $710 \pm 80\text{ }\mu\text{m}$ ), resulting in a rough surface and large particles of glass could easily be brushed off the surface. An experiment was designed using a finer glass powder ( $125 \pm 10\text{ }\mu\text{m}$ ) and varied amounts of glass powder pressed into the surface of an uncured silicone layer spread onto a fully cured silicone sheet.

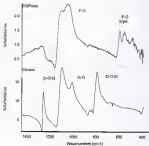


Figure 4-1: FTIR reflectance spectra for 5/5/Press. Blended glass powder coated silicon and an uncoated silicon disk reacted in HBT for 10 days at 17°C (compare with Table 2-2).

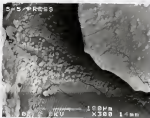


Figure 4-2b SEM micrograph of 1/2/1/2/2 surface reacted in H<sub>2</sub>O for 10 days at 17°C. Note that HCA (crystalline hydroxide) has formed on both the massive glass particles (left & right sides) and the silicate polymer (middle).

### 4.3 Varyed Amounts of Powder

Resistive glass coated samples were made with 0, 0.1-0.3, 0.4, 0.5 and 0.6 g of bioactive glass powder were fired in SHF for various times. Glass powder used on these samples was of a finer size range than before, 125 - 55  $\mu$ m. The glass powder on these samples was pressed into a layer of fused silicone applied to the surface and cured by using a heated carrier press. In addition, a sample called "0g" was made without pressing, by adding 0.6 g of powder and cured using a vacuum oven. Figure 4-3 shows FTIR analysis of an untreated silicone surface and a surface with 0.6 g of powder reacted for 20 hours in SHF at 77°C. Again the characteristic peaks of an SOA layer are present on the coated sample (bottom spectra) and not the untreated sample (top). One of the silicone peaks can be observed in the 0-0.6 g samples, a peak at 1258  $\text{cm}^{-1}$  for the Si-CH<sub>3</sub> bond vibration. The peak near 820  $\text{cm}^{-1}$  on the bottom spectra may be due to Si-O-Si from the formation of a silicagel layer during the reaction with SHF and not from the silicone polymer surface. A comparison of the amount of powder applied to the surface of samples reacted in SHF for 20 hours at 77°C is shown in Figure 4-4. The presence of a pair of peaks at 808  $\text{cm}^{-1}$ ,

representing the P-O crystalline bending vibrations and the wide P-O stretching vibration near  $1050\text{ cm}^{-1}$ , can be observed starting with 0.3 g sample and growing in strength with an increase in the amount of glass powder on the sample. Samples with 2.3 and 5.3 g of powder on their surface have little or no Raman is present (as represented by their FTIR spectra). Cross-section analysis of 2 sample imaged by low voltage SEM are shown in Figures 4-5 and 4-6. Cross-sections were made by breaking samples frozen in liquid nitrogen. Cross-sections of the 2.3 sample reveal that the majority of the bioactive glass particles are covered by silicone particles in the center of Figure 4-5 are covered by a layer of silicone present in their sight. This image is similar to what is observed with the 2.1 sample. Figure 4-6, shows a large number of particles exposed to the surface (top left of image) and is representative of what is observed with the 2.3, 2.4, and 5.3 samples. The results of this cross-sectional examination help explain the reasons for the differences observed in the FTIR analysis shown in Figure 4-4. Samples 0.1 and 2.2 present only a silicone surface. While, the 2.3, 2.4, and 5.3 samples present bioactive glass powder at their surfaces. SEM images of 20 hour reacted samples are shown in Figures 4-7 and 4-8.



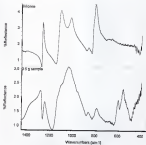


Figure 4-3

FTIR spectra of an untreated silicone sample and a sample treated with 0.5 g of dimethylsiloxane glass both released in DMF for 20 hours at 21°C

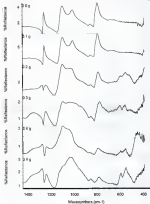


Figure 4-4 FTIR spectra of samples coated with 0, 0.1, 0.2, 0.3, 0.4, and 0.5 g of hexamethyldisiloxane powder and reacted in DHT for 20 hours at 170°C.

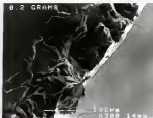


Figure 4-5: SEM image of the cross-section of a sample coated with 0.2 g bioactive glass powder (showing particles covered by silicate layer)

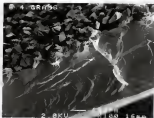
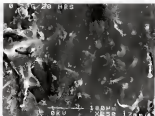


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SEM image of the cross-section of a sample coated with 0.5 g of blowing glass powder. (showing exposed particles on surface)



*Figure 10*

SEM image of the surface of a 3.5 sample reacted in DPF for 20 hours at 37°C. Note the lack of bioactive glass particles on the surface.

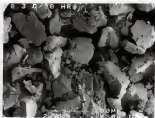


Figure 1-8 SEM image of the surface of a  $\text{SnI}_2$  sample coated in HEP for 20 hours at 37°C. Note the large number of bioactive glass particles on the surface

Figure 4-7 shows the surface of a 0.2 sample reacted OHF for 20 hours at 17°C. This surface shows few exposed bioactive glass particles and little reaction at the surface. In contrast, Figure 4-8 shows the reacted surface of a 2.2 sample, many bioactive glass particles are observed and the surfaces of these particles show HCA nodules and growth. These results correspond to what is observed with FTIR spectra of these surfaces. If no bioactive glass particles are exposed then there is no reaction at the surface to produce an HCA layer. Composites made using bioactive glasses and engineering thermoplastics are traditionally polished with 600 sand paper to expose the underlying glass from the matrix polymer (Khanb and Davis).

This difference is also observed by the change in elemental concentrations of phosphorus (P), silicon (Si), and calcium (Ca) in each reaction solution analyzed by inductively coupled plasma (ICP) spectroscopy. Figures 4-9, 4-10, and 4-11 show the concentrations of P, Si and Ca in solution, respectively, plotted for each time period and sample. Figure 4-10 shows a considerable drop in the P concentration for the 0.2, 2.2, and 2.5 samples, to levels that are much lower than the original 500 ppm concentration of 10.3 ppm. This phosphorus level reduction starts at the 2 hour time period and continues through the 20 hour period

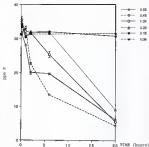


Figure 4-5: Plot of the phosphorus concentration (in ppm) in HMF solution reacted with 0. 0.1, 0.2, 0.3, 0.4 and 0.5 samples versus the time period (in hours) at 20°C.



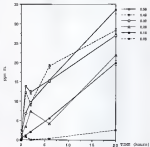


Figure 8-10: Plot of the silicon concentration (in ppm) on 99F solution reacted with 0, 0.1, 0.2, 0.3, 0.4 and 0.5 sampling versus the time period (in hours) at 27°C.

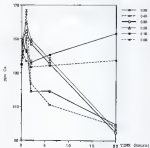


Figure 8-11: Plot of the calcium concentration (in ppm) in 3M EDTA solution reacted with 0, 0.1, 0.2, 0.3, 0.4 and 0.5 samples versus the time period (in hours) at 37°C.

This drop in the P level of reaction solutions has been associated, by many authors, with the precipitation and growth of an HCA layer on the surface of bioactive glasses (Klaft, Little, Rosta and Christ) and is preceded by an increase in the P level. This increase is associated with the leaching of phosphorus ions from the glass into solution. The observation of a drop in the P level beginning at the 2 hour reaction time period, was also reported by Kim et al. with 45S5 Bioglass® disks reacted in Tris buffer (Kim). This trend is not observed with the 0, 0.1, and 0.2 samples, except for the single 20 hour 0.2 sample. For the rest, the phosphorus level remained at or near the original 38F level, indicating that there was no precipitation of HCA on the sample surface. In addition, the same trends are also observed with the Ca levels plotted in Figures 4-10. An increase in the Ca level at the 1 hour time period, followed by a decrease to a level far below the original level in the 38F solution ( $135.9 \pm 2.2$  ppm). This trend being observed only for the 0.2, 0.1, 0.4, and 0.5 samples. The 0.2 and 0.5 samples remain at or near the original 38F level. The increasing trends observed in Figure 4-10 show that Si leaches from all of the glass coated samples and the amount of silicon that leaches into solution is directly related to the amount of glass coated

on the surface. Even the 9.1 and 9.2 samples leach small amounts of elemental silicon in to solution, contrary to the observation with SEM that this glass is covered by the silicone layer. However, images of the reacted samples shown in Figure 8-7, reveal that the surface has many defects that could allow limited access of the solution to the underlying glass particles. The 9.1, 9.3, and 9.4 samples all leached Si into solution at similar rates and leached much more Si than the 9.1 and 9.2 samples. The leaching of Si into solution by a bioactive glass, resulting in the condensation and repolymerization of a silicon-rich gel layer at the surface of this glass has been theorized as a mechanism for accelerating the nucleation and growth of the BCR layer that forms both *in vitro* and *in vivo* (Henfley).

### 8.1.2.2 Si "Sink" Effect

Kennelkamp et al., described the BCR reaction layer that formed around bioactive glass fibers embedded in a polycrystalline composite as a "sink" of bioactivity (2003). The authors reported that after 21 days *in vitro*, residues of a calcium phosphate layer (3-5  $\mu\text{m}$  thick) were observed using SEM in regions between 15 and 75  $\mu\text{m}$  surrounding the bioactive glass fibers. The following experiments were

established to determine if this effect would also occur with silicone samples. Both circular (C13) and rectangular (R13) shaped samples were made and tested. These samples had distinct areas coated with siloxane glass powder and etched areas (see Figure 4-12).

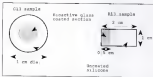


Figure 4-12: Diagram of C13 and R13 samples

Analysis of the surface, by FTIR, of C13 samples showed a similar result as the samples described in the previous section, an ROL layer formed on the surface after 1 day reaction in DMF (see Figure 4-13). These results only confirm the formation of an ROL layer on the reactive glass region. Low voltage SEM images revealed a new trend in the ROL formation (see Figures 4-14 through 4-17).

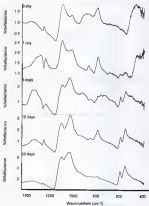


Figure 8-13 FTIR reflection spectra at the series of C13 samples treated in DMF for 0, 1, 5, 18 and 28 days at 37°C.



Figure 4-14 SEM micrograph of a section of C15 sample reacted in DMF for 20 days at 170°C. Note the lack of RCR growth on the silicone surface away from closely packed bioactive glass particles. A layer of RCR can be seen coating the particle surfaces.

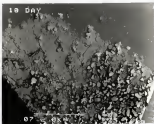


Figure 4-15. SEM micrograph of a section of tile sample treated in HF for 10 days at 77°C. Note that on the left, where glass particles are spread out, there is extensive growth of the HCA layer on the silicon surface. Growth is limited on the right, where particles are closely packed together.



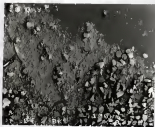


Figure 4-12: SEM micrograph of a section of C13 sample reacted in 5M for 10 days at 27°C. This is a magnified version of Figure 4-11.

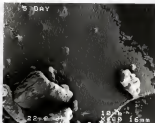


Figure 2-37. SEM micrograph of a section of the sample treated in XHF for 5 days at 37°C. Note the layer of BSA grown both on and between the glass particles.

The SEM micrographs shown in Figures 4-14 through 4-17, show a pattern of mixed RCA formation on silicon that has inactive glass particles spread apart and RCA formation limited to only the particle surface for closely packed particles. These results lead to a new theory that governs the formation of RCA between inactive glass particles (or regions). As the inactive glass particles leach long into solution, there forms a zone of leached ions around each particle. This leach zone is highly saturated with respect to phosphorus, silicon and sodium containing ions. If the particles are too close together leach zones overlap early in the inactive reaction causing precipitation of silicon and then RCA on the surface of the particles only. If the particles are too far apart then the zone grows until silicon and then RCA precipitate only on the particle. If the inactive particles are spaced just the right distance apart, then the separate leach zones for each particle grow until they overlap, at that point the solution is supersaturated, silicon and the RCA precipitate on both the particles and between the particles. In addition, the release of sodium such as  $Na^+$  and  $Na^+$  into the solution surrounding a glass particle through an ion exchange process, causes a localized decrease in pH, this pH decrease favors the precipitation of amorphous opaline (Fueh, 1960).

and Woodhill. This new distance theory of RCA formation between particles is being presented for the first time in this dissertation and is illustrated in Figure 4-18. This theory may explain trends that have been observed with composites made of bioactive material and thermoplastic engineering resins. When composites are made with 40% bioactive material, RCA is seen to form in veins on the surface of the bioactive material and rarely on the substrate surface (Woodhill and Woodhill). When higher concentrations of bioactive material are used, RCA forms over the entire sample surface. Examination of SEM micrographs published by these authors suggests that in composites made with 40% bioactive material, the particles (or regions) of bioactive material are spaced far apart from one another (Woodhill and Woodhill). Samples with higher amounts of bioactive material showed particles that were closer together. This theory may become important in composites made of bioactive material where the design of the device required maximum bioactivity at the surface with the least amount of bioactive filler material. Since the bioactive glass is the brittle phase of the composite, this would give a the desired tissue response while limiting the reduction in tensile strength and fracture toughness. A balance of properties is the ultimate goal of any composite material.

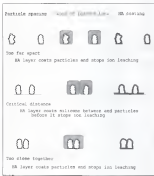


Figure 4-18: Diagram of BA precipitation distance theory

The variation of pH with distance from bioactive glass materials was presented in a recent study (Ghani). These authors studied various bioactive glasses and glass-ceramics by measuring the pH using a pair of ion-sensitive field effect transistors (ISFET) in direct contact with the material while immersed in BBP. An increase in the local pH, due to ion exchange, was observed after just a minute of immersion time for all the bioactive glasses. When the ISFET was moved away from the interface, the measured pH decreased to the original value of the BBP (Ghani). This decrease occurred at a point < 1 mm from the surface of the bioactive glass and suggests that the ion-exchange reaction is limited to the glass-BBP interface. The authors concluded that, since a higher pH favors RCA formation, the localized increase in pH at the glass-BBP interface decreases the partial solution of silica and the subsequent precipitation of RCA (Ghani).

The elemental concentrations of Ca, P and Na in solution as measured by ICP are shown in Figure 4-22. The points on each graph represent the mean of solutions from 3 separate samples (3 measurements each) and the error bar represents the standard deviation of that mean. As in the previous study, after 1 day the phosphorus level has decreased due to the precipitation of the RCA layer.

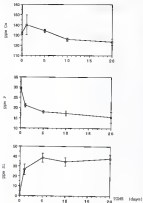


Figure 8-27: Plots of the elemental concentrations of calcium, phosphorus, and silicon in solutions of 887 reacted with C13 samples.

The Fe level also decreased below the original 987 ppm due to the HCA precipitation. The elemental Si concentration increased from 1.1 to a level near 34 ppm and remained at that level, suggesting that once the HCA layer precipitated on the surface of the glass particles the leaching of Si into solution is significantly reduced.

Uncoated silicones 1 cm disks (94) were reacted in HNF at 17°C for the same time periods shown as HCA formation by FTIR (Figure 4-22) or SEM (Figure 4-21). All HIL samples, due to their manufacturing process, had glass packed particles at the silicone/glass transition. These samples all reacted similar to those areas that had glass packed particles. SEM images were similar to Figure 4-18. FTIR and ICP analysis were omitted for these HIL samples.

### 4.3 Glass Samples

To further test the theory described in Figure 4-18, samples of silicone were coated with a pattern of individual Immature glass particles evenly spaced apart. Using a standard screen filtration such as a mask on the silicone surface, particles were allowed to contact the silicone surface only through the open areas on the mask. An SEM micrograph image of a Immature glass coated sample surface prepared in this manner is shown in Figure 4-23.



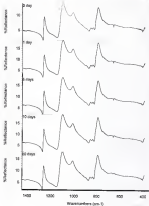


Figure 4-20: FTIR reflection spectra of annealed silicon samples treated in OBP for 0, 1, 3, 10 and 30 days at 57°C

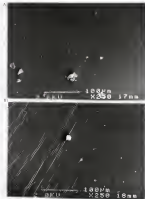


Figure 6-23. SEM micrographs of uncoated silicon samples reacted in 28F for A) 3 days and B) 10 days.



Figure 4-22 SEM micrograph of a sample made using a 70-mesh filtration mesh as a mesh. Note the evenly spaced glass particles on the surface.

The majority of the surface in Figure 4-23 has single floccative glass particles evenly spaced apart in rows. This sample was made using a very thin layer of uncured silicone, sized flocculant (185-55  $\mu$ m diameter), and a sylon 70  $\mu$ m screen mesh (thickness 70  $\mu$ m and 45% open area). A series of combinations of uncured silicone thickness, mesh size and particle size led to this coating method. If too thin a layer of uncured silicone was used, then the particles on the surface would dissolve away into the BSA during reaction. If too large a mesh size were used, then the sample would have small clusters of particles on the surface and reaction would be limited to only those clusters and not the silicone surface between the clusters.

Initial bioactivity testing isolated single samples tested at 1, 2, and 3 days in BSA at 37°C. SEM images of the surface of these "70 Mesh" samples revealed BSA growth both on the floccative glass particles and the silicone between them (shown in Figures 4-23, 4-24, and 4-25). This result was observed if the particles were less than 100  $\mu$ m apart. When individual particles were missing from the pattern, the BSA layer was not present on the silicone between the particles (see Figure 4-26). When two particles bordered an area with a missing particle, a bridging arc of BSA formation would be observed (shown at Figure 4-24).

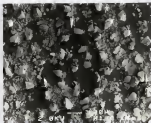


Figure 6-24: SEM micrograph of a 75 Bz sample reacted in BHT for 3 days at 175°C. Bz layers are the ones between particles that are 400 nm apart.

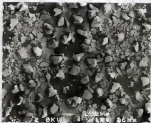


Figure 4-18. SEM micrograph of a 75 Mesh sample reacted in HMT for 3 days at 37°C. HCA layer can be seen between particles that are 4100  $\mu$ m apart. A circle of HCA can be seen on the border of a open area where a missing particle has caused a lack of HCA precipitation on the silicone surface.

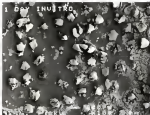


Figure 4-75: SEM micrograph of a 70 Mesh sample reacted in DGF for 1 day at 37°C. HCA layers can be seen beginning to form between particles in the upper left hand corner.

The center area of Figure 4-24, is barren of RCA and the border of that area is circled by an arc of RCA. Figure 4-25 shows a 70 Mesh sample that has been reacted for 1 day in RHF. In the upper-left hand corner there can be seen the beginnings of RCA precipitation between particles that are within the 100 um range. This is in stark contrast to the RCA formation that has occurred on the right side of the image; on the left side there is a cluster of 3 particles almost touching each other. The close proximity of these 3 particles may be a contributing factor to difference between the two sides. This same trend can be seen with the line of 3 particles in the top center of the image; these have also just started precipitating between them and the particles above them. FTIR images of the surface of these reacted samples are shown in Figure 4-26. At 1 days, the surface showed little RCA on the surface as measured by the presence of a pair of Si-O-Si stretching peaks at 810 and 570  $\text{cm}^{-1}$ . This results because 90% of the surface of the sample is covered by borosilicate glass particles. The rough surface of the particles and RCA growth areas scattered the light away in comparison to the smooth silicone which has more specular reflection and allows more of the silicone signal to reach the detector, giving a false reading of more silicone than RCA. Reacted silicone showed greater FTIR reflecting.



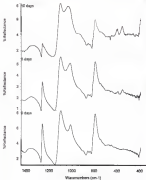


Figure 4-26b: FTIR spectra of TC Resin samples reacted in BAF for 0-, 3-, and 18 days at 37°C

Pd = 70 mesh sample is reacted for 10 days in HBF, then the pair of crystalline P-d peaks become much larger and the (100) (orthorhombic) peak at  $218 \text{ cm}^{-1}$  is reduced suggesting that most of the silicon is being covered by HCA.

To investigate the scope of HCA formation on these 70 mesh samples, 1 cm disks were made and reacted in HBF for 0, 1, 2, 7, 12, and 24 hours at  $37^\circ\text{C}$ . Elemental analysis of the concentrations of Ca, P, and Si in these HBF reaction solutions was performed using ICP and plots are shown in Figure 4-27. The data represent the mean of 3 sample solutions and the error bars represent the standard deviation of that mean. It must be noted that these solutions were the first to be analyzed using ICP and the Ca standard deviations were quite large. Refinement of the ICP method, by increasing the allowed time in ICP mode for the Ca measurement (from 800 msec), reduced this fluctuation in measurement. However, there was not enough solution left to treat these samples. The P level starts at that of HBF, increases slightly through the 1 hour time period and then decreases to a level much lower than HBF starting at 7 hours. This decrease is indicative of the P being consumed as part of the formation and growth of HCA on the surface. Although the standard deviations are high for the Ca measurements, the same trend can also be observed.

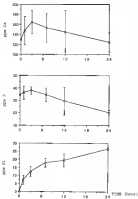


Figure 4-27: Plots of the eliminated concentrations of Ca, P, and Si in urine excreted with TE fluid samples for 1, 3, 7, 12 and 24 hours at 30°C

The level of  $\text{Ca}^{2+}$  in solution, seen in Figure 4-2F, changed at 0 and increases over the entire reaction period to a final value of  $24.4 \pm 0.3$  ppm.

#### 4.3 Samples 70/10, 70/20, 70/30, & 70/40

To further investigate the reactions that occur between 1 and 12 hours, samples were made of borosilicate glasses of various compositions using the same melt technique, described above. The compositions and  $\text{Ca/P}$  ratio of the glass powders used are show in Table 4-1. These borosilicate glass powders were obtained from O. F. Siematerials and had the designations 40a, 50a, 60a, and 80a.

Table 4-1: Borosilicate glass compositions.

	$\text{SiO}_2$ (mole%)	$\text{Na}_2\text{O}$ (mole%)	$\text{CaO}$ (mole%)	$\text{P}_2\text{O}_5$ (mole%)	$\text{Ca/P}$ ratio
40a	66.1	24.4	26.9	2.6	1
50a	62.1	20.8	29.8	2.6	4.4
60a	58.1	18.1	32.2	2.6	4.2
80a	48.1	17.1	19.6	2.6	3.6

Disks were made of each of these and named 70/10, 70/20, 70/30, and 70/40. These disks were reacted in both Tris buffer and HEP for 1, 7, 9, 18, and 12 hours. FTIR analysis of their surface revealed no significant changes

and is caused by the strong reflection from the smooth silicone surface, as discussed above. SEM images of the surfaces reveal that HSA precipitation had occurred both on and between the glass particles after 12 hours in SBF with the 70/30, 70/50 and 70/55 samples. Figures 4-29, shows the typical growth of HSA around the glass particles on a 70/45 sample after 12 hours in SBF. Continuous layers of HSA could be observed for particles that were  $<15 \mu\text{m}$  apart, and a distinct arc of growth is observed in the middle. In contrast, Figure 4-30 shows a 70/45 sample after 3 hours in SBF. No HSA growth was observed between the glass particles. Figures 4-30 and 4-31, show the typical growth on the surface of 70/50 samples after 12 hours in SBF. HSA growth was observed on and between the glass particles. Continuous growth was only seen when particles were  $<15 \mu\text{m}$  apart. Surrounding the large particle in the center of Figure 4-32, different amounts of HSA growth are seen; where particles are close continuous growth is seen and when distant spotty growth is observed. The typical surface of a 70/55 sample reacted for 12 hours is shown in Figure 4-33. Sparse HSA growth is seen between the glass particles on the surface. A 70/55 sample after 12 hours in SBF showed a total lack of HSA formation and the particle surfaces revealed silicon gel formation (Figures 4-33 and 4-34).

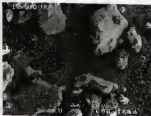


Figure 4-28: SEM micrograph of a 10/11 sample reacted in air for 12 hours at 37°C. BSA layer can be seen beginning to form between particles.

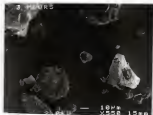


Figure 5-8 SEM micrograph of a 10/40 sample reacted for 200 hrs at 3 hours at 27°C. No IGA growth can be seen between particles.

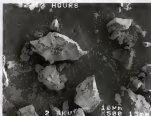


Figure 4-3b SEM micrograph of a 70/30 sample reacted in BHF for 12 hours at 37°C. SCA growth can be seen on and between the glass particles.



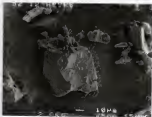


Figure 4-31. SEM micrograph of a 70/30 sample reacted in RBF for 12 hours at 37°C. RGA growth can be seen on and between the glass particles.

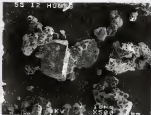


Figure 4-32- SEM micrograph of a Ti-55 sample removed in  
88P for 18 hours at 375°. Some oxide growth  
can be seen between the particles

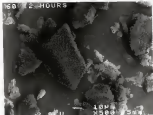


Figure 4-25: SEM micrograph of a 70/40 sample reacted in 200° Sox II for 24 hours at 37°C. The particular reaction surface shows only silica gel.

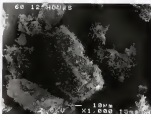


Figure 4-3d SEM micrograph of a TiO<sub>2</sub> sample reacted in H<sub>2</sub>O for 12 hours at 30°C. The silica gel layer connects particles together.

The square root of the distance between glass particles on the estimated percentage of silicate surface covered by HCA growth after 12 hours in DMF is plotted in Figure 4-23. These data were taken from the TEM micrographs shown in Figures 4-24 through 4-34. The distance was measured between solitary particles whose size ranged between 20 and 70  $\mu$ m by using a ruler and the wire bar located at the bottom right corner of the micrograph. Estimates of the percentage of HCA coverage were made by examining a 1  $\mu$ m wide section centered on a line spanning the distance between particles. This section was further divided into 1  $\mu$ m by 1  $\mu$ m squares, the number of squares that had HCA particles was then divided by the total number of squares between the particles to get a percentage. This method was used due to the lack of contrast between the two surfaces and it was a simple estimate of the coverage. The minimum distance for 100% HCA coverage was greatest for the 70/45 glass and decreased with increasing SiO<sub>2</sub> content in the glass (i.e., 70/45 > 70/52 > 70/55). A linear curve fit is plotted along with each of these compositions and gave the best  $r^2$  values 0.959, 0.991, and 0.998, respectively. Samples of 70/45 had no HCA formation on the glass particles themselves or on the fillers between them at any distance. The close linear correlation of a plot of HCA formation with the

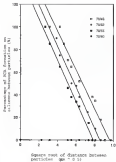
square root of the distance suggests that this reaction is a diffusion controlled process. The concentration of drug released from polymeric systems follows a similar relationship with release time and is shown in Equation 4-2 (Higuchi).

$$M_t/Q_\infty = k_d t^{1/2} \quad (4-2)$$

Where  $M_t/Q_\infty$  is the concentration,  $t$  is the time, and  $k_d$  is a diffusion constant. Time is proportional to the distance ( $x$ ) by the velocity ( $v$ ) of diffusion and therefore this equation is also proportional to the distance by Equation 4-2 (Higuchi),

$$M_t/Q_\infty = k_d t^{1/2} = k_d (xv)^{1/2} = k_d x^{1/2} \quad (4-3)$$

The diffusion control of the formation of RCA on silicones between dissimilar glass particles further supports the theory that a shell of leached ions exists around these particles. The linear curve fits for all 3 glass compositions have similar decreasing slopes with distance suggesting that the RCA formation is similar in each case and that the concentration varies with distance. The only difference is how far apart the 100% coverage extends for each composition suggesting similar diffusion coefficients with an effect due to the initial glass composition.



Figures 4-56, 4-57 and 4-58 give the elemental concentration of Ca, P, and Si (respectively) in SBF solutions as measured by ICP. Data points on each graph represent the mean of 3 reaction solutions (each with 3 measurements) for 70/40, 70/50, 70/60, 70/80 samples and uncoated silicone disks. The standard deviation of these means are represented as error bars on each data point. The lines connecting the points are drawn for clarification only. For the 70/40, 70/50, and 70/60 samples the Ca and P graphs have the same trend of an increase followed by a decrease in concentration as seen with the 70/80 sample in the previous section. The decrease is attributed to the precipitation and growth of HAp on the surface. Solutions from 70/80 sample had only small increases in the Ca and P levels but, no decrease after 12 hours reaction. The levels of Ca detected in solution increases in the same order as the amount of CaO present in the original glass composition (i.e.  $45 < 52 < 55 < 60$ ). This trend is not seen with the P levels since the amount of P<sub>2</sub>O<sub>5</sub> in each glass composition is the same. The levels of Si detected in solution increase inversely with the amount of SiO<sub>2</sub> in each glass composition (since with more SiO<sub>2</sub>, there less Na<sub>2</sub>O and CaO and are therefore more resistant to corrosion (Adachi and Sato); no essential change was observed with the uncoated silicone



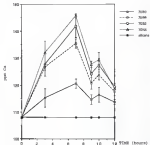


Figure 4-55. Plot of the elemental concentration of silicon in solutions of BPF reacted with 70/45, 70/50, 70/55, 70/60 and coated silicone diols for 0, 3, 7, 8, 10, and 12 hours at 17°C.

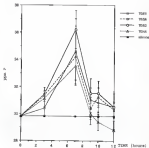


Figure 4-27 Plot of the elemental concentration of phosphorus in solutions of SF<sub>6</sub> reacted with 70/30, 75/25, 70/30, 70/30 and denuded silicone disks for 0, 3, 7, 9, 10, and 12 hours at 37°C.

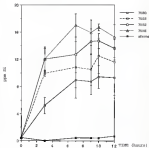


Figure 4-38: Plot of the elemental concentration of silicon in silicones of 34F treated with 7048, 78/82, 70/50, 78/60 and uncoated silicon chips for 0, 3, 7, 9, 10, and 12 hours at 10°C.

To check the accuracy the solution of various ions such as Ca and P, in the solution of these same glass compositions samples disks were also reacted in a fluid buffer devoid of Ca and P for the same time periods as above. Figures 4-25, 4-26 and 4-28 plot the elemental concentrations of Ca, P and Si (respectively) in this solution as measured by ICP. Open points and error bars on each graph again represent the mean and standard deviation of 3 reaction solutions (each with 3 measurements) for samples of 76/91, 76/92, 76/93 and 76/95. Samples of 76/94, 76/96 and 76/98 all showed an increase in the amount of Ca and P in solution with reaction time. In contrast, samples of 76/95 showed no increase in the Ca level and only a very small increase in the P level. The Ca level increases for 76/92 and 76/93 are in close agreement, increasing to ca. 4 ppm. Samples of 76/93 disks showed a larger increase in the Ca level (ca. 17 ppm). The increase in P levels for 76/92, 76/93 and 76/94 showed a very similar trend but, despite the fact that all 4 glass compositions had the same amount of P, samples from the 76/95 disks showed a much lower increase (ca. 3 ppm). The trend observed with the Si levels is not too dissimilar to the plot of the Si concentration in the fluid. The levels of Si dissolved in solution increased linearly in the amount of H<sub>2</sub>O present in each glass composition.

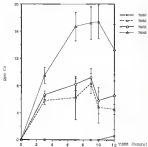


Figure 4-37- Plot of the simulated concentration of various species in solutions of Tris reacted with NO<sub>2</sub>, TBA, TBA, TBA and TBA for 0, 3, 6, 9, 10 and 12 hours at 10°C.

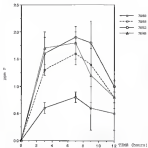


Figure 8-46 Plot of the elemental concentration of phosphorus in solutions of Tris reacted with 70/30, 70/50, 70/70 and 70/90 for 3, 6, 9, 12 and 15 hours at 17°C

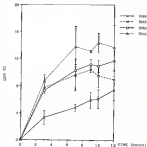


Figure 4-41. Plot of the elemental concentration of silicon in solutions of Triol reacted with 10/45, 10/55, 10/60 and 10/65 for 0, 3, 7, 9, 10 and 12 hours at 57°C.

Sampegas et al., measured the increase in surface area and average pore size with reaction time in Tris buffer for products of three same glass compositions and found that 85a glass had little change in both after 7 days (38a,b). The authors described the bioactivity of these glass compositions as: bonding to bone and soft tissues with 45a and 55a; bonding to bone only with 85a, and no bonding with 85b. The study concluded that the large increase in surface area observed with both 45a and 85a was responsible for the rapid HCA formation (25 hours) and bonding to both tissues, while the moderate surface area increase seen with 55a induced slow HCA formation (5 days) and only bone bonding. The small increase in surface area of 85b glass was not sufficient to induce HCA precipitation even after 20 days in Tris (38a,b). This increase contributes to glass corrosion observed with the 85a glass may be the reason for the lack of P found in the Tris solutions, the absence of HCA formation on either the glass or silicone surfaces, and the presence of only a silica gel layer on the reacted glass surface after 12 hours reaction (Figures 4-33 and 4-34). Studies have shown that silica gel surfaces can induce the formation of HCA after 3 weeks reaction in SBF at 37°C or when implanted in the bones of goats for 12 weeks (41a,b,c, 41d,e, 41f,g, and 41h,i).



The presence of a high surface area silica gel layer on the surface can induce HCA precipitation but, the presence of  $P_i$  in the glass influences the rate of HCA formation. The role of  $P_i$  in a glass matrix, on the rate of HCA precipitation was studied by Okazaki et al. (Okazaki). These authors found that a 50/50 CaO-SiO<sub>2</sub> glass would induce HCA to form in 3 days when reacted in SBF. In contrast the addition of 3 mole% P<sub>2</sub>O<sub>5</sub> to this glass shortens this time to 24 hours in SBF (Okazaki). Both a 50/50 CaO-P<sub>2</sub>O<sub>5</sub> glass and a 50/50/50 CaO-SiO<sub>2</sub>-P<sub>2</sub>O<sub>5</sub> glass showed no HCA formation even after 7 days reaction in SBF. All 4 of the glass compositions were reacted in SBF, a solution that is saturated with respect to hydroxyapatite (HAp) (40). ICP analysis by these authors showed that the reaction solutions showed a decrease in overall P level at the same time as the precipitation of HCA on the glass surface, indicating that did not induce HCA formation observed a steady increase in the P level through the duration of their reaction (Okazaki). The formation of a silica gel layer on the glass surface induces HCA formation, but a localized increase in the P and Ca level indicates this formation.

A one-way analysis of variance (ANOVA) statistical comparison of the ICP data from both the SBF and Tria solutions was performed using EXCEL (version 2.0).

GraphPad Software, San Diego, CA). Comparisons were made between the 4 glass compositions for each time period, element (Ca, P and Si) and solution. The results are presented in Table 4-3. In addition, a multiple pairwise post test using a Student's *t* test was performed to compare each of the compositions, if the *P* value was  $\geq 0.05$ .

Table 4-3: Results of ANOVA statistical comparisons (*P* values  $\geq 0.05$  are bold).

SRF solution			
	Ca levels	P levels	Si levels
3 hours	$P = 0.0013$	$P = 0.0090$	$P = 0.0008$
7 hours	$P = 0.0010$	$P = 0.0700$	$P = 0.0010$
9 hours	$P = 0.0004$	$P = 0.0070$	$P = 0.0071$
20 hours	$P = 0.0010$	$P = 0.0100$	$P = 0.0004$
12 hours	$P = 0.0009$	$P = 0.0110$	$P = 0.0010$
Tris buffer solution			
3 hours	$P = 0.0001$	$P = 0.0010$	$P = 0.0001$
7 hours	$P = 0.0001$	$P = 0.0008$	$P = 0.0010$
9 hours	$P = 0.0001$	$P = 0.0010$	$P = 0.0001$
14 hours	$P = 0.0001$	$P = 0.0040$	$P = 0.0005$
12 hours	$P = 0.0008$	$P = 0.0710$	$P = 0.0100$

Reaction among the compositions was significantly greater than expected by chance ( $P < 0.05$ ) for all the time periods with the Ca and Si levels. The trends and differences observed with these 2 elements are statistically

significant throughout the reaction period studied. The variations among the compositions for the F levels is somewhat more complex, all the glasses have the same amount of F in them and should not be different. For the HF solutions, statistically significant differences were observed with later reaction periods (i.e. after 5 hours). Review of the multiple pair-wise comparison shows that the differences observed after 5 hours are found between the TL/50 disks and the other sample disks, these differences are therefore due to the reduction in the F level caused by the formation and growth of the continuous SiO<sub>2</sub> layer on the TL/50 disks. For the Tris solutions, the opposite is true, significant differences are seen at early reaction periods and not after 5 hours. The pair-wise post test revealed that the differences are observed between the TL/50 disks and the other samples. Early leaching of this corrosion resistant glass composition had very small F levels that were near the detection limit of F for ICP (0.2 ppm). The lack of resolution at these low levels could be responsible for the differences observed.

A statistical comparison of the increases in Cu, F and Si levels in HF (above HF base-line) and Tris was performed pair-wise for each element, time period and glass composition using a Welch unpaired approximate t test.

There was no statistically significant difference found between the increase in HF and Tria for elemental P or Si (average  $F = 3.3077$  and  $0.3384$ ). A statistically significant difference was not observed between the increase in Ca levels of HF vs. Tria solutions (average  $F = 0.8644$ ). Therefore common ions had little or no effect on the amount of Ca and P leached from the glass into the surrounding solution. These results are included in appendix A.

#### 2.3 Fine Reacting Glass Powder

Recently, U.S. Silsilicals Corp., started manufacturing Suprasil® powder in a size range that had never before been made. This very fine size powder was made by using a "jet mill", a milling machine that uses very high pressure liquid gas to create a vortex inside a stainless steel container. Glass powder is introduced into this vortex and centrifugal forces cause the larger particles to move to the outer edge of the vortex, while the very smallest particles are allowed to reside in the center and exit the container. Particle-particle collisions at the outer edge of the vortex cause the glass particles to break apart. Once small enough, these particles exit through the center of the vortex. Size is controlled by the pressure of the gas creating the vortex and the number of times a powder

is passed through the series. The 41st Runcland particle size ranges obtained from S. S. Sinterstake were:  $< 0.5 \mu$ ,  $< 1 \mu$  and  $< 2 \mu$ . Feeders were spread on sheets of silicone that were coated with a thin layer of uncured silicone ("T" samples) and uncoated silicone sheets ("W" samples). Preliminary tests had suggested that the uncured silicone might not be necessary for these fine sized particles. There was not the case. Disks made by reacting with fine glass particles only and no uncured silicone showed a total dissolution of the particles and a business after 24 hours reaction in 2HF but, FTIR analysis revealed no RCA on the surface of the disks. It is still unclear what reactions took place on the surface to produce the lumpy appearance observed. Disks made with the thin layer of uncured silicone did produce a RCA coating on their surface and showed little dissolution of their particles (Figure 4-42). Figures 4-43, 4-44, and 4-45 show the reaction surface of disk of  $< 0.5$ ,  $< 1$  and  $< 2 \mu$  particles reacted for 24 hours in 2HF. Above are disk with the silicone layer (T), disks without 2H, and uncoated disks. Disks with the thin silicone layer show the formation of an RCA layer on their surface, represented as the F-O peaks at  $608 \text{ cm}^{-1}$ . Disks without the silicone layer and the uncoated disks do not.



Figure 4-12 Photograph of N-20 disk and Y-20 disk reacted in 50% D<sub>2</sub>O 24 hours at 37°C. With the unreacted milligram Y sample the particles remain and without the particles are dissolved into solution.

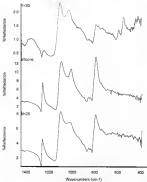


Figure 4-43 IR spectrum of disk with the silicone layer 9-20, uncured silicone, and without the silicone layer. IR spectrum was recorded in N<sub>2</sub> for 24 hours at 30°C.

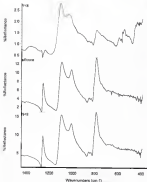


Figure 4-44: FTIR spectrum of disk with the silicone layer P-R, uncured silicone, and without the silicone layer R48 reacted in 50% for 24 hours at 30°C.



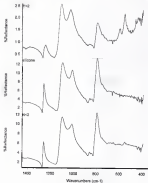


Figure 4-45: FTIR spectrum of disk with the silicone layer B-2, coated silicone, and without the silicone layer B-2 reacted in DMF for 24 hours at 37°C.

Figures 4-6a, 5-17 and 7-20 show the elemental concentrations of Ca, P and Si respectively in SRP reaction solutions as measured by ICP. Data points on each graph represent the mean of 3 reaction solutions (each with 3 measurements). These graphs show that the T samples (with the thin layer of silicone) have much higher Ca and Si levels than the B samples (without silicone layer). This result suggests that the T samples may have more glass powder than the B samples and careful examination of the sterilized samples under light microscopy revealed that in fact the T samples did have bi-layers and sometimes tri-layers of powder on the surface covering the thin silicone layer. Only a mono-layer of glass powder was observed on the B samples. Comparing the T samples together shows close equivalent and the same is true when the B samples are compared together. The formation of RCA on the T sample surfaces can be related to the increase followed by decrease in both the Ca and P levels. Again the P levels drop to a level well below the original SRP level, suggesting that P is being used from the SRP to grow the RCA layer on the surface. No significant difference was measured between the different sizes of glass particles with respect to the levels of elemental Ca, P or Si in solution. This may be due the presence of similar sized particles in all 3 samples.

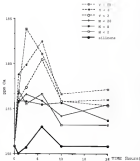


Figure 4-15 Plot of the effect of concentration of calcium on rate of polymerization at 17°C. Curves for 0, 1, 2, 5, 10 and 24 hours at 17°C.

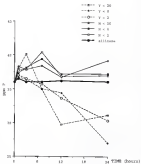


Figure 4-47: Plot of the dimensional compression of phosphorus in solutions of BHF recorded for 2, 5, 12, 18 and 24 hours at  $37^{\circ}\text{C}$ .

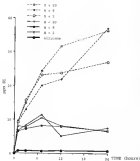


Figure 4-65: Plot of the aluminum concentration of various solutions of  $\text{HClO}_4$  treated for 0, 1, 2, 4, 8, 12 and 24 hours at  $30^\circ\text{C}$ .

### 4.2 pH Measurements

Throughout these experiments the pH of each solution was measured at 37°C after having reacted with the samples. Measurements were made at 37°C due to an observation that the increase in pH between room temperature (ca. 25°C) and 37°C was as high as 0.5.

In no case during this study did the pH of buffer as this buffer reacted with these samples increase more than the error of the pH probe ( $\pm 0.05$ ). This result is in contrast to the results obtained by other researchers studying Bioglass® amorphous samples in vitro (Bartl, Ogilvie, Oakes, Kokke, Macfie, Mills and Smith). In all these other cases the ion exchange occurring at the glass surface was identified as the cause of the increase in solution pH. This ion exchange has been shown to produced silica-rich leach layers at the glass surface reported to be as thick as 50  $\mu\text{m}$  (Bartl). This reaction layer has been shown to become as thick as 300  $\mu\text{m}$  in vivo (Winkler). A gel layer that thick would be greater than the total size of the particles on the surface of our samples. Therefore, the lack of a pH increase in our studies is due to 2 related reasons: 1) the amount of buffer solution used is too large to observe a change in pH due to small amounts of ions being leached from

the particles and 2) the majority of ions leached from solution are used in the formation and growth of the SO<sub>2</sub> layer on the surface of these samples. The latter reason is also supported by the reduction in the solution ion concentration of Ca and P.

#### 4.2 Dip Coating of Catheters

Several combinations of soak time and silicone/benzoate concentration were tested to produce the coated layer shown in Figure 4-2B. Too much time or too high a concentration of silicone in the dipping solution resulted in a coated catheter with no bioactive glass exposed to the surface. Too little time or too low a concentration of silicone would result in an exposed glass coating that could easily be removed by gentle rubbing. Before coating excess solution was allowed to drip off the sample and the benzoate was allowed to evaporate.

The resulting surface has bioactive glass particles imbedded in the final cured siloxane surface. These glass particles can only be removed by scraping with a sharp blade. They will not rub off. The catheter material is still flexible, can be bent without particles flaking off and remains flexible even after 3 days in DMF at 37°C.



Figure 4-14. SEM micrograph of the cross-section of a broken catheter piece that has been coated with bioactive glass powder using a dip coating technique with 5% silicic acid/saline



## CHAPTER 5 CONCLUSION AND FUTURE WORK

### 5.1. CONCLUSIONS

This study has shown that the formation of hydrogen-bonded epitaxial (HBE) on the substrate surface between lithium glass particles is a function of the particle size, composition and the distance between particles. The formation follows a diffusion controlled process with the rate proportional to the square root of the distance ( $d^2$ ) between particles. The composition of the glass determines the off-set of this relationship. This conclusion can explain why compositions made of only 12 to 30% lithium glass show formation of HBE on the glass particles and not between them (BenNir). SEM micrographs revealed that the particles on these compositions were indeed too far apart to form HBE between them.

In all cases the concentrations of Ca and F in solution decreased with the HBE formation on the surface. This represented a consumption of these ions for the formation and

growth of the apatite layer. This fact, coupled with the observation described above suggests a new theory that the formation of HCA on the surface was the result of a zone of leached ions present surrounding the glass particles. The concentration of this zone is dependant on the distance from the particles, and once a critical concentration is reached, formation of HCA occurs. The formation occurs first as an amorphous apatite layer and is converted into a crystalline HCA layer. This trend is similar to that observed for the formation of hydroxyapatite from saturated, moderately supersaturated and electrolyte solutions (Gronth, Fan'9, and Wright).

This study was unable to observe a common ion effect on the total leached ions in solution. This may have been due to the localized nature of the formation of HCA on the surface and the limited effect that this formation had on the bulk solution. The limited effect was also observed as a lack of increase in the overall solution pH over the duration of this study.

This study has also shown that composites made of bioactive glass and silicone must have the glass exposed at the surface to be bioactive. This result is in contrast with a patent that describes a bulk sized hydroxyapatite and silicone composite with excellent tissue adhesion (Frank).

## 1.2 Future Work

First, the effect of bioactive glass coatings on peritoneal catheters needs to be examined *in vivo*. Long-term animal studies in either sheep or dogs seems to be the accepted model for this type of study. Special attention during implantation should be focused on the tightness of the seal at the exit-site, the rate of infection at the exit-site, and any extrusion of the catheter. Histological analysis after completion of the study would play a key role in determining the amount of epidermal downgrowth exhibited. Catheters both with and without neuron cuffs still attached should be included in these experiments. The cuff may still be used to anchor the catheter in place for long-term stability.

Second, if this type of coating is successful then it need not be limited to peritoneal catheters. Hemodialysis catheters and other percutaneous access devices could make use of it. Fever catheters for other implants may also benefit from a coating like this. In addition, drug delivery depots made of silicone implants could have improved release profiles. Currently, these devices form a fibrous capsule around them. This capsule is not well

vacuolized and a barrier to drug release. Implants that have direct soft tissue adhesion may not have this barrier to release and may improve the release profile of the drug.

# APPENDIX A HEAVY DATA

Heavy-Pair Production,  $\tau\tau$ , 0-10 and 4-12.

mean values in $\mathcal{B}\mathcal{B}$ (ppb) $\pm$ statistical deviation (ppb)							
name	0-5 y	0-5 y	0-5 y	0-5 y	0-5 y	0-5 y	etc.
20-hour	89.6 $\pm$ 0.33	89.6 $\pm$ 0.44	89.6 $\pm$ 0.18	89.6 $\pm$ 0.83	183.6 $\pm$ 0.33	183.6 $\pm$ 0.44	189.6 $\pm$ 0.46
4-hour	139.0 $\pm$ 0.49	163.0 $\pm$ 0.33	139.0 $\pm$ 0.44	120.7 $\pm$ 1.4	148.4 $\pm$ 0.33	139.0 $\pm$ 1.2	111. $\pm$ 1.1
3-hour	139.0 $\pm$ 0.74	133.0 $\pm$ 0.33	141.1 $\pm$ 0.2	149.0 $\pm$ 0.44	129.3 $\pm$ 1.2	133.0 $\pm$ 0.74	110.1 $\pm$ 0.7
1-hour	150.2 $\pm$ 1.4	145.0 $\pm$ 1.4	154.4 $\pm$ 0.44	150.4 $\pm$ 0.74	140.0 $\pm$ 1.2	134.0 $\pm$ 1.2	144.0 $\pm$ 1.7
10-min	148.0 $\pm$ 0.47	148.0 $\pm$ 1.1	148.0 $\pm$ 1.1	148.0 $\pm$ 0.4	147.0 $\pm$ 0.44	148.0 $\pm$ 0.44	148.0 $\pm$ 0.4
0-hour	139.0 $\pm$ 0.2	133.0 $\pm$ 0.2	133.0 $\pm$ 0.2	136.0 $\pm$ 0.2	129.0 $\pm$ 0.2	134.0 $\pm$ 0.2	140.0 $\pm$ 0.2
mean phosphorus in $\mathcal{B}\mathcal{B}$ (ppb) $\pm$ statistical deviation (ppb)							
20-hour	8.0 $\pm$ 0.04	8.0 $\pm$ 0.10	7.5 $\pm$ 0.15	8.0 $\pm$ 0.10	10.7 $\pm$ 0.07	11.4 $\pm$ 0.10	8.0 $\pm$ 0.18
4-hour	10.0 $\pm$ 0.19	13.4 $\pm$ 0.04	10.0 $\pm$ 0.10	11.7 $\pm$ 0.10	10.0 $\pm$ 0.4	11.0 $\pm$ 0.10	14.0 $\pm$ 0.10
3-hour	10.0 $\pm$ 0.44	10.0 $\pm$ 0.10	11.7 $\pm$ 0.10	11.0 $\pm$ 0.10	10.0 $\pm$ 0.44	11.0 $\pm$ 0.17	12.0 $\pm$ 0.12
1-hour	10.0 $\pm$ 0.17	11.0 $\pm$ 0.44	10.0 $\pm$ 0.10	10.0 $\pm$ 0.10	10.0 $\pm$ 0.10	10.0 $\pm$ 0.44	10.0 $\pm$ 0.10
10-min	10.0 $\pm$ 0.07	11.7 $\pm$ 0.10	11.0 $\pm$ 0.10	10.0 $\pm$ 0.10	10.0 $\pm$ 0.10	11.0 $\pm$ 0.10	11.0 $\pm$ 0.10
0-hour	10.0 $\pm$ 0.1	10.0 $\pm$ 0.1	10.0 $\pm$ 0.1	10.0 $\pm$ 0.1	10.0 $\pm$ 0.1	10.0 $\pm$ 0.1	10.0 $\pm$ 0.1

Mean concentration in 100 ppm $\pm$ standard deviation (ppm)							
	0.5 g	0.1 g	0.2 g	0.3 g	0.1 g	0.5 g	0.1
0.5 hour	13.5 $\pm$ 4.0	18.0 $\pm$ 5.40	24.5 $\pm$ 5.10	22.5 $\pm$ 5.10	13.5 $\pm$ 5.40	18.0 $\pm$ 5.40	40.5 $\pm$ 5.10
1 hour	14.5 $\pm$ 5.2	19.0 $\pm$ 5.10	24.5 $\pm$ 5.10	24.5 $\pm$ 5.10	14.5 $\pm$ 5.10	19.0 $\pm$ 5.10	14.5 $\pm$ 5.10
2 hours	23.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	23.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10
3 hours	19.0 $\pm$ 5.1	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10
4 hours	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10
5 hours	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10
6 hours	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10	19.0 $\pm$ 5.10

Data for Figure 4-19:

Mean concentration in 100 ppm $\pm$ standard deviation of 3 samples			
	ppm Cu	ppm P	ppm S
0 day	121.8 $\pm$ 1.4	20.8 $\pm$ 0.8	0.7 $\pm$ 0.3
1 day	140.0 $\pm$ 1.3	21.3 $\pm$ 0.8	24.3 $\pm$ 5.2
5 days	134.2 $\pm$ 1.5	18.0 $\pm$ 0.6	18.5 $\pm$ 0.6
10 days	129.8 $\pm$ 1.4	17.3 $\pm$ 1.1	24.5 $\pm$ 4.2
20 days	123.3 $\pm$ 1.3	15.4 $\pm$ 2.5	37.7 $\pm$ 4.4

Data for Figure 4-21:

Mean concentration in 100 ppm $\pm$ standard deviation of 3 samples			
	ppm Cu	ppm P	ppm S
1 hour	147.0 $\pm$ 20.3	20.3 $\pm$ 5.5	7.1 $\pm$ 3.7
3 hours	144.4 $\pm$ 20.3	21.0 $\pm$ 3.0	12.4 $\pm$ 3.0
7 hours	153.8 $\pm$ 20.3	24.5 $\pm$ 5.5	15.8 $\pm$ 3.9
12 hours	144.2 $\pm$ 40.3	25.4 $\pm$ 13.3	18.4 $\pm$ 4.0
20 hours	124.2 $\pm$ 14.3	20.2 $\pm$ 1.0	16.8 $\pm$ 0.9

Data for Figure 4-35

Estimated % RCA coverage as measured from 600's after 12 hours					
diameter (mm)	rate (%)	T8/T5 (%)	T6/T5 (%)	T8/S5 (%)	T6/T6 (%)
0	0				0.0
5	2.234				0.0
7	2.644			100	
12	3.182		100	85	0.0
15	3.613		90		
18	4.243	100	75	45	
22	4.89	85			
28	5.688	71		44	0.0
32	5.477	65	50	38	0.0
34	4		48	34	
40	4.325	52	38	30	0.0
52	7.321		25		0.0
54	7.348			25	
60	7.748	38		0	0.0
65	8.582	30	10		
75	8.64	28	0		
82	8.13	0			
90	8.747				0.0

Data for Figures 4-36, 4-37, and 4-38.

mean sodium in HEP (ppm) $\pm$ standard deviation (SD) of 3 samples normalized to sodium chloride					
	10:00	10:15	10:30	10:45	unknown
3 hours	132.2 $\pm$ 3.4	130.0 $\pm$ 3.5	127.7 $\pm$ 4.4	128.2 $\pm$ 4.5	128
7 hours	128.0 $\pm$ 3.7	125.4 $\pm$ 3.7	121.5 $\pm$ 4.0	123.7 $\pm$ 3.9	122
9 hours	124.2 $\pm$ 3.4	126.7 $\pm$ 3.3	124.1 $\pm$ 3.0	127.5 $\pm$ 3.4	126
10 hours	126.0 $\pm$ 3.2	123.0 $\pm$ 3.2	121.4 $\pm$ 3.4	126.5 $\pm$ 3.7	124
12 hours	123.7 $\pm$ 3.9	123.0 $\pm$ 3.3	121.4 $\pm$ 3.1	126.0 $\pm$ 3.0	124
mean phosphate in HEP (ppm) $\pm$ standard deviation (SD) of 3 samples normalized to sodium chloride					
3 hours	34.4 $\pm$ 0.4	35.0 $\pm$ 0.3	35.4 $\pm$ 0.4	35.1 $\pm$ 0.3	35.0
7 hours	34.0 $\pm$ 0.3	34.2 $\pm$ 0.1	34.0 $\pm$ 0.4	35.5 $\pm$ 1.2	34.0
9 hours	35.0 $\pm$ 0.3	35.8 $\pm$ 0.3	35.0 $\pm$ 1.1	36.1 $\pm$ 0.3	35.4
10 hours	35.0 $\pm$ 0.7	35.3 $\pm$ 0.7	35.0 $\pm$ 0.4	36.1 $\pm$ 0.3	35.5
12 hours	35.3 $\pm$ 0.5	35.0 $\pm$ 0.4	35.3 $\pm$ 1.0	36.1 $\pm$ 0.1	35.3
mean sodium in HEP (ppm) $\pm$ standard deviation (SD) of 3 samples					
3 hours	5.0 $\pm$ 1.2	5.0 $\pm$ 0.4	5.0 $\pm$ 0.4	5.0 $\pm$ 0.4	5.4
7 hours	5.0 $\pm$ 1.1	4.0 $\pm$ 0.5	5.0 $\pm$ 0.3	5.0 $\pm$ 0.7	5.4
9 hours	5.0 $\pm$ 1.0	4.0 $\pm$ 0.3	4.0 $\pm$ 0.3	5.0 $\pm$ 0.3	5.4
10 hours	5.0 $\pm$ 1.7	4.0 $\pm$ 0.4	5.0 $\pm$ 1.0	5.0 $\pm$ 0.5	5.4
12 hours	5.0 $\pm$ 1.1	4.0 $\pm$ 0.3	5.0 $\pm$ 1.7	5.0 $\pm$ 0.3	5.4



mean value is  $\frac{1}{n} \sum_{i=1}^n \bar{y}_i$  and standard deviation is  $\frac{1}{n} \sum_{i=1}^n \bar{y}_i^2$ .

mean value is $\frac{1}{n} \sum_{i=1}^n \bar{y}_i$ and standard deviation is $\frac{1}{n} \sum_{i=1}^n \bar{y}_i^2$				
	$\bar{y}_1/\bar{y}_2$	$\bar{y}_3/\bar{y}_4$	$\bar{y}_5/\bar{y}_6$	$\bar{y}_7/\bar{y}_8$
3 hours	4.4 ± 0.3	5.4 ± 0.4	6.4 ± 0.4	7.5 ± 1.2
7 hours	4.4 ± 0.3	6.2 ± 0.5	6.7 ± 0.4	10.5 ± 1.1
9 hours	4.4 ± 0.3	6.5 ± 0.5	6.7 ± 0.5	12.2 ± 0.4
10 hours	4.4 ± 0.3	6.5 ± 0.5	6.8 ± 0.4	12.4 ± 0.5
11 hours	4.4 ± 0.3	6.5 ± 0.5	6.8 ± 0.3	13.5 ± 0.7
mean phosphorus on Test buffer (ppm) ± standard deviation of 3 samples				
	$\bar{y}_1/\bar{y}_2$	$\bar{y}_3/\bar{y}_4$	$\bar{y}_5/\bar{y}_6$	$\bar{y}_7/\bar{y}_8$
3 hours	4.4 ± 0.3	5.4 ± 0.3	5.4 ± 0.3	5.7 ± 0.2
7 hours	4.4 ± 0.3	5.4 ± 0.3	5.7 ± 0.3	5.8 ± 0.2
9 hours	4.4 ± 0.3	5.5 ± 0.4	5.7 ± 0.4	5.8 ± 0.3
10 hours	4.5 ± 0.3	4.4 ± 0.3	5.7 ± 0.3	5.8 ± 0.3
mean value is $\frac{1}{n} \sum_{i=1}^n \bar{y}_i$ and standard deviation of 3 samples				
	$\bar{y}_1/\bar{y}_2$	$\bar{y}_3/\bar{y}_4$	$\bar{y}_5/\bar{y}_6$	$\bar{y}_7/\bar{y}_8$
3 hours	5.3 ± 0.3	7.7 ± 0.5	7.7 ± 0.4	8.7 ± 0.3
7 hours	6.3 ± 0.5	9.4 ± 0.7	10.7 ± 0.5	12.7 ± 0.4
9 hours	6.4 ± 0.2	10.4 ± 0.4	11.7 ± 0.7	12.3 ± 0.3
10 hours	6.3 ± 0.4	9.5 ± 0.4	10.7 ± 0.4	14.4 ± 0.4
11 hours	7.4 ± 0.5	9.4 ± 0.5	11.7 ± 0.5	15.7 ± 0.5

Data for Figures 4-66 and 4-67:

mean nitrate in 200 (ppm) ± standard deviation of 5 samples					
	2 hours	3 hours	7 hours	12 hours	24 hours
N = 30	270.2 ± 4.2	282.6 ± 26.7	185.2 ± 2.0	189.6 ± 23.4	274.6 ± 2.1
N = 6	274.8 ± 4.4	279.2 ± 4.0	187.4 ± 3.0	187.2 ± 2.1	248.0 ± 7.5
N = 3	286.4 ± 3.4	278.2 ± 3.4	185.6 ± 2.4	187.6 ± 3.4	244.8 ± 4.6
N = 30	247.6 ± 3.0	249.7 ± 22.7	127.4 ± 0.0	142.0 ± 0.0	142.2 ± 2.7
N = 6	247.2 ± 3.7	247.4 ± 3.0	140.2 ± 1.0	140.0 ± 2.7	141.1 ± 0.5
N = 3	272.6 ± 4.4	244.4 ± 2.1	129.8 ± 0.4	154.4 ± 2.1	126.4 ± 0.4
allison	198.6 ± 0.2	192.8 ± 3.8	158.8 ± 5.2	142.6 ± 5.2	112.6 ± 5.2
mean phosphate in 200 (ppm) ± standard deviation of 5 samples					
N = 30	37.6 ± 2.8	48.2 ± 2.8	58.4 ± 0.4	24.7 ± 4.8	34.6 ± 1.2
N = 6	34.2 ± 0.7	34.4 ± 0.1	55.0 ± 0.0	24.4 ± 2.0	37.0 ± 0.0
N = 3	37.6 ± 0.4	34.6 ± 0.0	55.7 ± 2.7	32.4 ± 0.4	30.0 ± 1.7
N = 30	34.6 ± 0.4	37.6 ± 0.0	58.4 ± 0.2	24.7 ± 0.0	34.6 ± 0.0
N = 6	37.2 ± 0.1	34.6 ± 0.0	55.4 ± 0.0	27.0 ± 0.0	37.0 ± 0.0
N = 3	37.7 ± 0.2	37.6 ± 0.0	62.4 ± 0.0	28.8 ± 0.4	34.6 ± 0.0
allison	34.6 ± 0.7	34.6 ± 0.0	58.8 ± 0.0	28.2 ± 2.0	34.6 ± 0.0

Table 10: Same as 979

mean value at 200 Speed $\pm$ standard deviation of 3 samples					
$n = 10$	9.9 $\pm$ 0.4	14.8 $\pm$ 0.3	18.2 $\pm$ 0.3	20.8 $\pm$ 0.4	18.0 $\pm$ 0.3
$n = 8$	9.5 $\pm$ 0.4	14.8 $\pm$ 0.4	18.9 $\pm$ 0.3	20.8 $\pm$ 0.4	18.9 $\pm$ 0.3
$n = 3$	9.3 $\pm$ 0.3	15.4 $\pm$ 0.4	20.5 $\pm$ 0.3	20.3 $\pm$ 0.4	18.9 $\pm$ 0.3
$n = 100$	9.8 $\pm$ 0.4	9.3 $\pm$ 0.3	11.3 $\pm$ 0.3	9.0 $\pm$ 0.3	7.8 $\pm$ 0.3
$n = 8$	9.4 $\pm$ 0.3	7.3 $\pm$ 0.3	9.3 $\pm$ 0.4	7.8 $\pm$ 0.3	9.8 $\pm$ 0.3
$n = 3$	9.4 $\pm$ 0.3	9.3 $\pm$ 0.4	10.4 $\pm$ 0.3	9.5 $\pm$ 0.3	9.8 $\pm$ 0.3
alliance	9.8 $\pm$ 0.3	9.0 $\pm$ 0.3	9.0 $\pm$ 0.3	9.8 $\pm$ 0.3	9.8 $\pm$ 0.3

Data for common ion statistical analysis

Expanded student's t test between 2 means

(two-tailed P values)

Are the increases in BPF values equal to Tm buffered values?

	3 hours	7 hours	9 hours	10 hours	11 hours
10/50 samples					
P	0.0018	0.1071	0.0000	0.0000	0.7040
SL	0.1000	0.0070	0.1000	0.0000	0.1000
Cu	0.0000	0.0411	0.0047	0.0000	0.0070
10/50 samples					
P	0.0070	0.1400	0.0000	0.0000	0.400
SL	0.0010	0.7000	0.0000	0.0000	0.1000
Cu	0.0000	0.0014	0.0000	0.0070	0.0000
10/50 samples					
P	1	0.0000	0.0000	0.0000	0.0000
SL	0.0000	0.1000	0.0000	0.0000	0.1000
Cu	0.0000	0.0000	0.0000	0.0000	0.0000
10/95 samples					
P	0.0000	0.0000	0.0000	0.0000	0.0000
SL	0.0000	0.0000	0.0000	0.0000	0.0000
Cu	0.0000	0.0000	0.0000	0.0000	0.0000

APPENDIX B  
LIST OF PUBLICATIONS

3. Reuch, M., Lefort, G., Bouvier, P., Baudin, J.,  
Nollens, E., Properties of quaternary optical  
matrices with 4.5 nm and 5.5 nm pores. *Proc SPIE-Int  
Soc Opt Eng* 1756 34-36, 1992.

Abstract:

Sn2-pot processing of tetra-Me orthosilicates with HSO<sub>4</sub> as a catalyst was used to make optically transparent silica matrices with interconnected porosity of 1.2 to 1.4 nm radii. However, larger pores are often needed for impregnation of the matrices with optically active organo-larger pore resins. Two methods for producing larger pore matrices are compared. (I) catalysis with OsO<sub>4</sub>, H<sub>2</sub>O<sub>2</sub> and (II) aging in a basic NaOH solution. Pore radii of matrices made by the H<sub>2</sub>O<sub>2</sub> method are 5.5 nm after thermal stabilization at 900° and 4.4 nm after 1800°. Pore radii are 0.8 nm/kg at 900° and 0.7 nm/kg at 1800°. The ammonia aging process yields 5.5 nm radius pores at 900° and 4.5 nm pores at 1800°. Optical properties (including UV cut-off, 25°-90° film transmission, IR absorption, index of refraction, bulk and structural densities of the matrices made by both methods (900° and 1800° stabilization) are compared with the 1.4 nm pore radius matrices.

4. Baudin, J., Coudane, D., Balogh, C., Surface changes in "silicone" elastomer upon exposure to sodium.  
*Proceeding Society for Biomaterials Annual Meeting*,  
148, 1994.

Abstract:

Silicones have been used extensively in plastic and reconstructive surgery for the past 30 years. Their use has been in the form of elastomers, oils, and gels, with the most common silicone being polydimethylsiloxane, i.e. PDMS. Approximately 1 million valves in the United States currently have silicone breast implants, composed of gel and elastomer PDMS. PDMS has generally been assumed to be biologically inert because of its oxidation and thermal stability, and nonadhesiveness to tissues. This is due in part to the fact that PDMS is one of the most hydrophobic polymers known. Recently the biocompatibility of PDMS has been under question and its possible interactions with

the immediate withdrawal of some of great interest. It was noted that PMSI elastomers slowly become hydrophilic when exposed to saline for long times, and the following study examines this in more detail.

Sections of PMSI medical grade ELASTATION sheathing (8 1/2" thickness) were cleaned in a sonicating bath of ultrapure water (Millipore system) for 15 minutes, rinsed twice and allowed to air dry. These samples were then maintained in vacuum for 48 hours using a Schlier extractor to remove any low molecular weight siloxanes.

Samples were then placed in a 0.5M saline solution at temperatures of 80°, 70°, 60°, and 100°C. A Pyrex® brand organic reaction vessel with a modified still lid was used. Reactions were started with one PMSI sample and additional samples were added at subsequent times to make 1, 3, 10, 20, and 40 hour treatment samples. After 48 hours all samples were removed and rinsed twice with ultrapure water and allowed to set in a ultrapure water storage bath for one hour. Samples were then analyzed using contact angle goniometer and X-ray photoelectron spectroscopy (XPS).

Perfluorooctyl tri-methoxypropylsiloxane was used to derivatize samples for analysis by XPS. XPS derivatization is an indirect measurement of the silanol concentration on the PMSI surface but is needed, since an oxygen atom bonded to a silicon atom would appear the same whether in the backbone or in a silanol configuration. As well, the vacuum needed for XPS could cause the silanol to return into the backbone again. After treating samples in saline solution and rinsing with ultrapure water, they were placed in a 0M solution of Perfluorooctyl alcohol and allowed to sit for 18 minutes. Samples were then rinsed with ethyl alcohol and cured in a desiccator for 24 hours at room temperature. High resolution XPS scans for C1s, O1s, Si1F and Si1S were made of the samples. The atomic concentration of nitrogen is assumed to be related to the concentration of silanol groups present on the PMSI surface.

Four control experiments were performed to determine the effect of the reaction vessel on the changes of PMSI samples. The first control used a Pyrex® brand organic reaction vessel with the PMSI sample folded over and held by clamp rings. Saline solution was injected between the folds of PMSI and this setup was placed in the reaction vessel. The second control used a poly(methylpentene) i.e. PMP volumetric flask, the third used the PMP flask and 10 grams of PMP fragments in the flask, and the fourth used the PMP flask and 10 grams of glass fragments in the flask.

Having PEG siloxane as a silane siloxane cavity, is a hydrophilic surface measured by contact angle goniometer). This is believed to be caused by the hydroxyl linkage of the siloxane linkage (see Fig. 1); silanol groups are formed on the surface of the PEG siloxane.

This reaction follows an Arrhenius relationship. The activation energy of the reaction can be derived from the slope of this Arrhenius plot. This activation energy can then be used to calculate the time required to achieve a hydrophilic surface at body temperature, 37°C.

The concentration of silanol groups on the surface of the PEG was estimated using two techniques, contact angle goniometry and XPS derivatization. Regression analysis of contact angle and XPS [18] data was used to determine the silanol concentration on the surface. Controls of untreated PEGs were used as 0% silanol concentrations. Arrhenius plots of this data determined the activation energy required for the production of silanol groups on the surface of treated PEGs.

The activation energies calculated through these two methods were in close agreement, 4.4 kcal/mol for the contact angle goniometry and 4.1 kcal/mol for XPS derivatization. These values are in agreement with those found in the literature for a catalyzed thermal decomposition and a catalyzed silane-siloxane of PEGs[3-4]. From the various control experiments, on the effects of the container used, it is believed that the surface silanol group concentration is due to the hydrolytic degradation of the PEG and not the deposition of glass on the PEG surface.

From the activation energy determined in this study, the time dependency for the formation of silanol groups on the surface of PEGs at body temperature can be calculated using the following equation:

$$[\text{SiOH}] = k \ln(t) + [\text{SiOH}]_0, \quad \text{where } k = E_a \times e^{-E_a/RT}$$

Because of the logarithmic function of the equation, a short initial exposure time produces a large change in the fractional surface coverage by silanol groups, from just over 1% for 12 hours to 33% in one month (making several assumptions about 'full' surface coverage).

It is clear that much additional work needs to be done to characterize the possible hydrolysis of PEGs in the body, before a complete understanding of this phenomenon is possible. These experiments were conducted using one type of highly filled PEG. The effect of this filler on the

properties of HMB is currently being studied. These results, alternative explanations, and possible implications will also be discussed.

1. Ya, M., Lefterov, G., Margolis, J., Barish, C., Nardi, M., *In vitro* measurements of silicone bleed from breast implants. *Plast Reconstruct Surg* 57 784-788, 1975

#### Abstract

A method to measure gel bleed from intact silicone gel-filled breast implants was developed. This nondestructive technique permits accurate and reproducible serial measurement of silicone bleed from smooth wall breast implants (PMO) under simulated physiologic conditions *in vitro*. Gel bleed rates from new low bleed gel-filled implants and intact explants (unbarriered, low bleed, double lumen) were determined. These results demonstrate the reliability of this method to quantify silicone gel bleed and may permit a meaningful comparison of bleed rates from implants in the future.

2. Barish, C., Lefterov, G., Margolis, J., Lefterov, G., Nardi, M. Silicone degradation reactions. *Curr Top Microbiol Immunol* 110 17-22, 1976
3. Klemm, J., Margolis, J., Nardi, M., Barish, C. Surface properties of Foley catheters: relationship to bacteriuria and fouling. *Proceedings Fifth World Biomaterials Congress*, 176, 1976

#### Abstract

A variety of Foley catheters are currently available: latex, 100% silicone elastomer, polyvinyl chloride, hydrogel coated latex and silicone coated latex catheters are among the variety of products at the disposal of the medical industry. For several reasons, silicone elastomer coated (SEC) latex catheters are the most commonly used of these alternatives.

SEC catheters have been shown to possess the advantages of lower inflammatory response and lower bladder infection. However, the rates of catheter-induced bacteriuria and colonization are not significantly reduced when SEC catheters are used in lieu of standard latex catheters.

The goal of this study was to examine the interior and exterior surfaces of SEC catheters to determine their morphology and confirm or deny the presence of silicone.



a study relating cathode morphology to the rates of bacteriolar and sporulation in naturally occurring.

SEC catheters, size 14 or 16 F., were obtained from the sales representatives for four different worldwide distributors of Foley catheters. Two catheters from each of the four manufacturers were dried under vacuum for 14 hours. Dried catheters were frozen in liquid nitrogen and then broken in half. This method was chosen in preference to cutting with a blade since it is the belief of the authors that the latter technique may lead to artifactual delaminations of the silicone from the latex. Samples were selected at random and spatter coated with carbon using a Techniques Research V sputter coater. EDX's were obtained of the interfacial regions between the latex and the silicone of the luminal surface using a JEOL JSM 4100 scanning electron microscope. A second set of catheters (N-SEC) from one of the manufacturers was treated in a similar manner. The manufacturing process for these catheters had been modified to produce a smooth layer of silicone on the luminal surface.

EDX's were examined by 3 blinded judges. The judges studied the photos to determine whether there was silicone present, and if present, to measure the thickness of the layer.

No silicone was found on the luminal surfaces of two of the four brands of catheters. The silicone which was on the luminal surface of the other two brands was thin and did not present a smooth surface. The mean thickness of the silicone layer in these brands was 1  $\mu$ m. The surface morphology observed in most brands was composed of large scale ridges (approximately 100 $\mu$ m) with smaller cavities within. N-SEC catheters presented a thin (1  $\mu$ m), smooth silicone layer on the luminal surface.

Anderson and others have represented the view that roughened surfaces may serve as sidi for the formation of fucating crystals. Additionally roughened surfaces may provide a better medium on which bacterial proliferation may occur. Considering that fuculating microorganisms are the premier causative agent in bacteremia, the large scale holes and defects seen on the luminal surfaces may serve to provide favorable localized hypoxic areas in which these organisms may multiply.

Bendall, et al, and Bousia, et al, have not been able to show a significant difference between pure latex and silicone coated latex catheters when they studied their rates of bacteremia. Additionally, other authors have obtained debatable results when they compared the rates of bacteremia in SEC and latex catheters. It is likely that

the catheters used in these studies may not have had an adequate coating of silicone on their internal surfaces. We admit that if the internal surfaces of the catheters are adequately coated, that HEC catheters may behave in a manner similar to that seen with pure silicone catheters.

A histohistochemical study to confirm or deny these hypotheses is currently underway. The results of this additional study will also be presented, deny the presence of silicone. A study relating surface morphology to the rates of bacteriostasis and encrustation is currently underway.

4. Baehria, J. LaFerre, SP. Batich, C. Bader, RM, Ye, L. Mechanisms of silicone in tissue sites both adjacent to and distant from ruptured and intact silicone breast implants. Proceedings Fifth World Biocompatibility Congress, 1978, 1979.

#### Summary:

The transport of silicone fluid to tissue sites distant from the tissue capsule, surrounding silicone breast implants, is a subject of great controversy. Detection techniques have been used to quantify the levels of elemental silicon (Si) in the capsules surrounding both intact and ruptured silicone breast implants.

The purpose of this study was to quantitatively measure the levels of silicon in tissues of rabbits with ruptured and intact silicone breast implants and infer from this the loading of silicone in these tissues.

Eight rabbits were implanted with 3 groups of breast implants (Ethex, Hestec, Corp.): 20 intact silicone gel-filled; 20 intact saline-filled; and 20 ruptured silicone gel-filled. Rabbits were sacrificed for periods between 3 months and 3 years. The following organs were removed for analysis: brain, capsule, heart, kidney, liver, lungs, pancreas, spleen, and regional nodes. Five unimplanted rabbits were used as controls. Sections of each organ were taken for pathological analysis. The remaining tissue was weighed, digested in 2 vol% HNO<sub>3</sub>, and the resulting solution was then analyzed with inductively coupled plasma (ICP) spectrometry.

A total of 375 samples were analyzed to determine the concentration of elemental silicon (ppm Si or ppb Si/dL). These concentrations were then converted to micrograms polydimethylsiloxane (PDMS)/gram tissue. Comparison of rates of occurrence of elevated PDMS levels (i.e. greater than control mean plus 2 standard deviations) among ruptured, intact and saline groups was performed (Fisher's exact test). Rates differed significantly among the 3

groups for blood tissue (P=0.011) and spleen tissue (P=0.042). A significant decreasing tissue blood in values from ruptured to intact to saline was noted for the breast tissue (P=0.035).

1. **Harmon, J.** LeFevre, G., Ketch, G., Herdt, H., Yu, L. Measurement of gel blood from silicone breast implants. Proceedings Fifth World Biomechanical Congress, 179, 1984.

#### Abstract:

Silicone gel consists of an insoluble crosslinked polymer and a mixture of lower molecular weight soluble soluble components. The diffusion of these soluble components through the implant shell and into the surrounding tissue is known as "gel bleed". This group has developed a non-destructive technique that permits accurate and reproducible serial measurements of silicone "bleed" from intact breast implants under simulated physiologic conditions. A total of 38 implants, removed from patients after removal, were tested in vitro at 2 week intervals for a period of 18 weeks.

The purpose of this study was to identify any significant differences in the bleed rates between types of implants.

A wide range of ages and manufacturers of breast implants were tested and include untextured gel-filled (GOF), low bleed gel-filled (low) and double layer gel-silicone (DLS) implants. Implants were immersed in a 1:1 implant volume to solution volume of simulated body fluid (SBF) that was maintained at 37°C for 2 weeks. At each 2 week interval Truine 8-100 was added to the solution, the implant & solution agitated for 30 minutes, the implant removed & rinsed with deionized water, and then the implant placed in a new jar containing fresh SBF. The concentration of elemental silicon (ppm Si) for each of these solutions was then measured using inductively coupled plasma (ICP) spectroscopy.

Silicone bleed levels for pairs of implants from the same patient were similar. No statistically significant trend was seen in the implant bleed rates vs- the age. Average values obtained were  $11.8 \pm 6.1$  ppm Si/2 week for the GOF,  $14.8 \pm 4.8$  for the low, and  $20.4 \pm 7.0$  for the DLS. The range observed was from 4.8 to 32.8 ppm Si/2 week. A slight statistical difference (P = 0.042) between the types of implants studied was observed.

8. Wilson, J. Martin, J. Cohen, B. Batley, J. Materials used in urological devices. *Journal of Long-Term Effects of Implants* 7:1-28, 1987

**Abstract:**

The most commonly used materials in the manufacture of urological devices are discussed with respect to their application to urinary catheters, penile implants, testicular implants, artificial urinary sphincters, and urological stents. The manufacturing, physical properties, and general chemical and biological behavior of these materials are reviewed. Attention is paid to future research trends and the general conditions of the field of urological device materials.

9. Goldberg, EP, Wickham, C, Martin, J, Martin, P. Failure of silicone gel breast implants: analysis of titanium data for 1983 explanted prostheses. *Plant Research* Supp. 308/280-284, 1987.
10. Martin, JH, Goldberg, EP. Estimation studies with breast implant silicone elastomer shells and "gels" indicate very high concentrations of soluble uncross-linked silicone. *Proceeding Society for Biomaterials Annual Meeting*, 332, 1987.

**Abstract:**

So-called "gels" used in silicone gel-filled breast prostheses are not true gels in that these are actually compositions containing a minor amount of lightly cross-linked PMS swelling with low molecular weight PMS oil. The properties of such "gels" are therefore greatly dependent upon their actual compositions. The soluble components of the PMS elastomer shells are also important. Swelling estimation was performed on samples of elastomer shell and gel from silicone gel-filled breast implant materials and implants.

Migration of oil from the gel through the shell and into the body is referred to as "gel bleed". Estimates of the amount of soluble PMS oils have ranged from 20% to 50% of the "gel" and the PMS fluid is very soluble in the cross-linked silicone elastomer shell surrounding the gel. In a sense, silicone gel-filled prostheses may be regarded as "controlled silicone release" implants and it is therefore important to know the composition of the "gels" and elastomers which have been so poorly identified to date.

Silicone gel in this study was obtained from 3 unimplanted prostheses and 4 explanted pairs of silicone breast implants. Implant ages were 3, 4, 13, 15, and 19 years. Explanted specimens were sterilized with ethylene oxide prior to gel recovery. Specimens of elastomer shell were carefully dissected to obtain samples for water studies. Two samples of elastomer shell from a few were cut from each shell for extraction analysis. "Isis" were removed and stored at room temperature in clean polypropylene containers.

Elastomer samples were partly covered with lint-free tissue to remove any superficial gel. Extraction of the "gel" involved adding 1-4 grams of weighed gel to a suitable extraction thimble and then placing an additional thimble on top to create a sealed extraction thimble. This assured that no gel would float out during the extraction process. Extractions were performed using chloroform and were carried out until no further weight loss was detected in each sample (usually 3 days for the implant shell and 7 days for the implant gel). The values reported represent the soluble fluid portion of silicone in each of the samples. In the case of the shells, the suitable fraction isolates fluid that has diffused or "bled" into the shell during storage and/or implantation.

Two gel samples and two shell samples from each implant were analyzed. The range of weight % extracted was: control shells 2.8-18.7%, explant shells 3.1-15.7%, control gels 18.4-91.7%, and explant gels 41.7-86.2%. The control shell extraction values are twice those previously reported by Fink and Goldstein (4 weight loss of original unfilled shells, CSI, Inc.)<sup>2</sup> Our values may be due to the fact that our control shells were stored gel-filled and silicone solvents from the gel diffused into them. The explant shell extraction values are twice the control values and could be a result of elastomer degradation and/or prolonged *in vivo* contact with gel for many years. The gel extraction values of all the implants, with the exception of the 19 year old explants, were much higher (84-94%) than previously reported. Gel extraction values for the 19 year old explants (80-89%) were lower than any other gel extraction values. This may result from the fact that early implants were filled with a more adhesive (more highly cross-linked) "gel". More recent implants were reportedly filled with gels that had more silicone oil added by manufacturers to give the "gels" a more "natural feel".

Implant gel contraction values are much higher than those suggested by the implant manufacturers, as high as 66% uncontracted PDB. This means that the amount of available silicone available for gel "bleed" is much greater than previously suggested.

A greater amount of available oil in the gel would mean that more oil is available to bleed from the implant while in the body.<sup>2</sup> Silicone oil that bleeds from implants may then be carried away by cells to other parts of the body.<sup>3,4</sup> The effect of this oil as a possible stimulus to immune problems is still under debate. Yet, swelling of the elastomer shell by the fluid component of the gel can result in a reduction of the elastomer tensile strength.<sup>5</sup> An FDA panel in 1980, commented that higher fluidity of implant gel implied "faster movement of liquid silicone from within the gel zone to the shell and through the shell" and in the case of a ruptured implant "larger amount of shrapnel could disperse from the exposed gel mass and dissipate throughout the body."<sup>6</sup> At that meeting, it was also noted that the lack of specifications for silicone gel manufacturers would result in gels of variable consistencies and compatibilities. In this regard, our study affords new data concerning the compositions of silicone implant elastomers and "gels".

11. WOODHOUSE, CH, BARNES, JH, BIRK, JF, HENRY, SP, HARRIS, R, MARTIN, P, SCHUBERT, SP. Comprehensive protocol for characterization of explanted silicone gel breast prostheses. Proceedings Society for Biomaterials Annual Meeting, 173, 1987.

#### Abstract.

Silicone gel breast implant safety remains controversial. As increasing numbers of implants are explanted, it is important to develop a sound data base to track the possible deterioration of properties that may lead to ruptures and other complications. A comprehensive physical and mechanical property test and evaluation protocol has therefore been developed for analysis of silicone gel breast implant controls and implants. Key aspects of the protocol and some preliminary data for 3 control and 11 explanted prostheses are presented here.

Visual and tactile appearance and integrity of the prostheses are observed and photographed prior to separating the gel from the shell. The elastomer shell is carefully cut into various samples for further analysis.

Mechanical properties are evaluated using tensile and tear testing, and dynamic mechanical spectroscopy (DMR). The tensile testing uses ASTM D 412-B; die C samples as a

model 1122 Instron, with a strain rate of 18 in/min. The same instrument is used for ASTM type 3 tensile testing (ASTM D 874-91). A Dine 180 thermal analysis system is used for DSC analysis with sample dimensions of 4mm length and 7-12 mm width.

The gel flow (viscosity) properties are evaluated by a method we developed utilizing a Tissue Well Flow Indicator. Soxhlet extraction with chloroform is used to determine the soluble fraction of silicone within the gel and elastomer shell. Observations of the silicone shell surface morphology, integrity, topography and appearance are made using optical, low voltage scanning electron, and atomic force microscopy (OM, SEM, and AFM).

Sample integrity for explants ranged from intact samples with no visible shell defects, 1 of the 12 which were ruptured, one explant shell (58-15 years) was completely obliterated, and some explants required very gentle handling to avoid tearing. The appearance, test, and composition of the gel was variable, with some explants having very tacky and viscous gel, discolored, and unidentifiable opaque inclusions. Some control samples contained foreign debris.

Tensile testing clearly identified a significant decrease in strength of the elastomer shell with time following implantation. For example, a decrease of 54-87% at 4 years. Tear strength of the explanted elastomers seemed strongly dependent on shell thickness and results will be reported when approximately 10 explants have been evaluated.

DM analysis readily identified thermal transitions for the various silicone materials. The  $T_g$  (-112 to -117°C),  $T_m$  (-34 to -41°C), and a barrier layer  $T_g$  (-64 to -72 °C) were seen.

Our newly developed Gel Flow Index (GFI) method used in this protocol provides reliable quantitative measurement of the gel flow properties at physiologic temperature, and appears clearly superior to previously used crude techniques.<sup>1</sup> The reproducibility of the method allows statistical comparison of sample data.

Soluble fractions removed from the gel by Soxhlet extraction in chloroform ranged from 43% (21) to 94% (58), and fractions removed from the elastomer shells ranged from 1% (2-1) to 27% (28).

A high degree of variability was observed for these initial samples, and the comprehensive battery of physical, tactile, and mechanical analysis techniques is necessary for a thorough evaluation of explants. DM is a useful additional tool for determining the dynamic behavior and thermal transitions, providing information on the composition and thermomechanical properties of the silicone

shell materials

The gel flow rheology has been characterized by a new method, GFI Analysis. Viscosity and flow properties of the gel can be reliably measured by this technique.

Soluble fractions increase with implant time, and control values were found to be twice those reported previously by Ficks and Delamater.<sup>1</sup>

The overall protocol, as demonstrated by initial test data, appears sound for characterization of silicone gel mammary prosthesis implants and explants.



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## BIOGRAPHICAL SKETCH

James Keith Harotta was born at Mobile Army Hospital, Ft. McPherson, Anniston, Alabama, on May 27, 1928. Ft. McPherson has the distinct honor of being one of the few facilities in the world that still train lime mortar apert and biological weapons. His father was stationed there as a captain in the Army Chemical Corp., and his mother was a nurse at a local hospital.

In 1942, his family moved to Leesburg, Florida, where he lived until graduating from Tavares High School in 1946. After enlisting in the Florida Army National Guard, he was sent to Ft. Benning, Georgia, for Infantry Basic Training and Individual Advanced Training. During his 4 years of military service, he received 4 promotions, the Army Service Ribbon, several Company Certificates of Appreciation, an Army Certificate of Achievement, Florida Military Affairs-Certificate of Appreciation and the Reserve Overseas Ribbon for service in the Republic of Panama. During his National Guard service, he attended Lake Wales Community College where he met Dr. Edmund Carver, a chemistry teacher that sparked his interest in chemistry.

After service in the National Guard, James moved to Gainesville, Florida, to attend the University of Florida. He was thrust into deciding a major after only 1 semester by the infamous "90 hour rule." He always enjoyed reading about exploration of space and space-craft so, he took a copy of his transcripts to the aerospace undergraduate adviser and ask to be admitted to their program. At that time his only grade from the University was a C in Physics and admittance to the aerospace department was denied. He had to find a major or leave the University. Knowing that he wanted to pursue an engineering degree, he took his transcripts to each undergraduate adviser (in alphabetical order) and asked for admittance. Each one only looked at the sole University grade and denied his admittance except Dr. CURTIS of Materials Science and Engineering. He was admitted on a probationary agreement and that semester received 3 A's and 1 B+. One A was received in Numerical Methods a class taught by Dr. John Mahoney, the undergraduate adviser for industrial and systems engineering, who had said that James "did not belong in engineering."

After obtaining his Bachelor of Science in Engineering from the University of Florida, James was admitted to the graduate program. In August of 1952, James began his



graduate studies under the supervision of Dr. Christopher G. Schick. While working in the area of biomaterials, he has performed a host of different projects involving several different medical devices from Foley catheter testing for an international medical device firm to the design of an in vitro blood test and destructive testing of explanted breast implants.

I certify that I have read this study and that in my opinion it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy



Christopher S. Eick, Chairman  
Professor of Materials  
Science and Engineering

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William E. Johnson  
Associate Professor of  
Materials Science and  
Engineering

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Eugene F. Golikoff  
Professor of Materials  
Science and Engineering

I certify that I have read this study and that in my opinion it conforms to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy



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Graduate Research Professor  
of Materials Science and  
Engineering

I certify that I have read this study and that my opinion is conformable to acceptable standards of scholarly presentation and is fully adequate, in scope and quality, as a dissertation for the degree of Doctor of Philosophy.

  
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This dissertation was submitted to the Graduate Faculty of the College of Engineering and to the Graduate School and was accepted as partial fulfillment of the requirements for the degree of Doctor of Philosophy.

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